

# CQA Certification Report

## Don Tyson Parkway Interchange

### Sunray #1 Landfill Final Cover Reconstruction

Class 1 Landfill

AFIN: 72-00144

September 2014

Project No. 35139161



**Prepared for:**

Garver, LLC  
2049 E. Joyce Blvd., Ste. 400  
Fayetteville, Arkansas 72703

**Prepared by:**

Terracon Consultants, Inc.  
25809 Interstate 30 South  
Little Rock, Arkansas 72022  
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Rec'd Digitally

AFIN: 72-00144

PMT#: 0123-SR-2

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## PROFESSIONAL ENGINEER'S CERTIFICATION

"I certify to the best of my professional judgment that the final cover system for the Sunray #1 Landfill located at the Don Tyson Parkway Interchange in Springdale, Arkansas was constructed in accordance with Arkansas Department of Environmental Quality regulations and the Work Plan dated March 29, 2012 and approved by email from Bryan Leamons (ADEQ SWMD) to Dave McCormick (Terracon Consultants, Inc.) dated March 30, 2012, except where noted. This certification is contingent on the fact that all information supplied to the signatory authority, at the time of this certification is unquestionably accurate and was provided in good faith."



---

F. Owen Carpenter, P.E., P.G.  
Arkansas Professional Engineer No. 8653

Oct. 3, 2014  
Date

Terracon Certificate of Authorization No. 223

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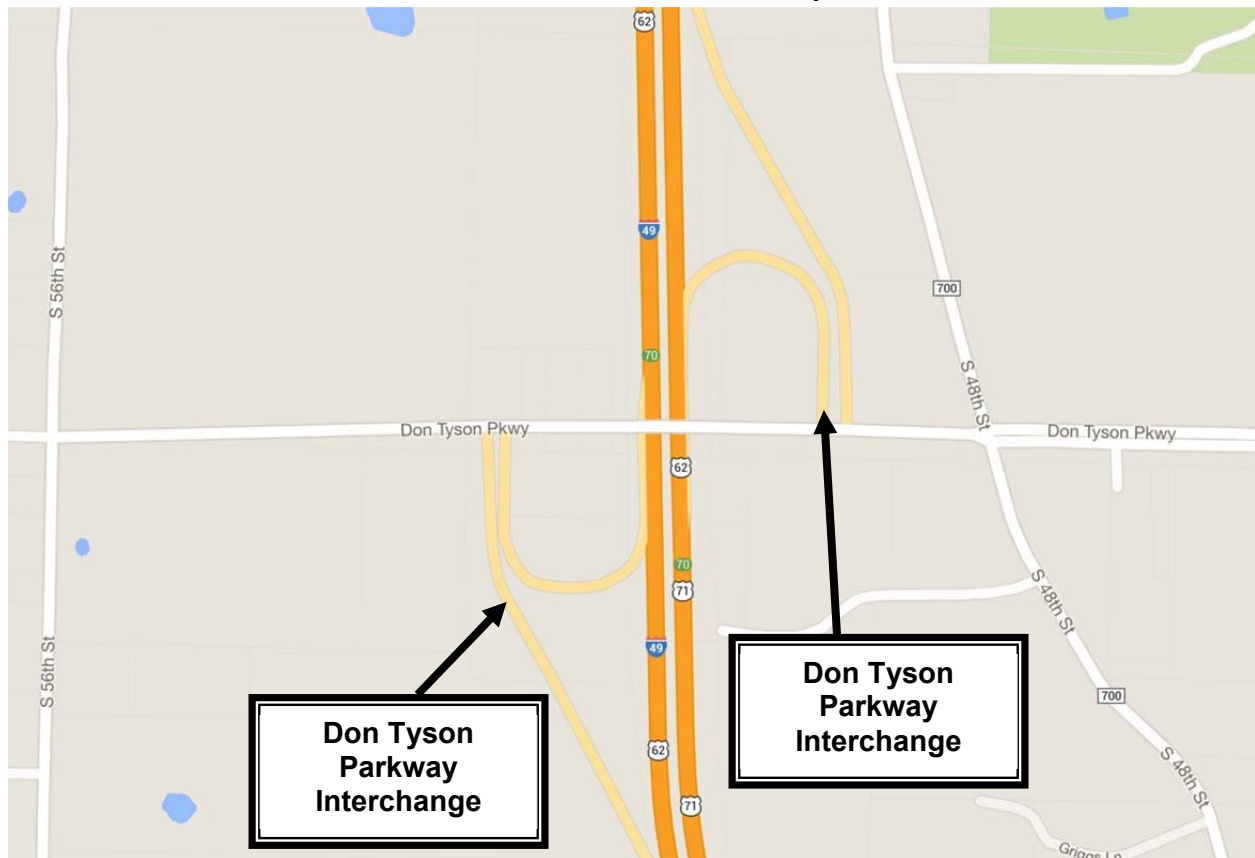
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## 1.0 INTRODUCTION

This construction quality assurance (CQA) report summarizes testing and documentation activities performed by Terracon Consultants, Inc. (Terracon) during the construction of the final clay cover system work associated with the Don Tyson Interchange located in Springdale, Arkansas. **FIGURE 1 - Site Location Map** below illustrates the geographic location of the site.

**FIGURE 1 Site Location Map**



This document summarizes the construction of the compacted clay cover (CCC) portion of the final cover system. Correspondence, details, quality control test results, and certifications associated with the construction have also been provided in the Appendices. This document, in conjunction with project as-built drawing, is intended to satisfy the requirements of the *Arkansas Department of Environmental Quality (ADEQ) Regulation 22.428*.

### 1.1 General

The construction of the compacted clay cover for the closed Sunray Landfill was conducted in accordance with the following documents:

- “Regulation Number 22, Solid Waste Management,” by Arkansas Department of Pollution Control and Ecology, Solid Waste Management Division
- *Work Plan* prepared by Terracon Consultants, Inc. and submitted to ADEQ for approval in March 2012.

## 1.2 Site Description

Two existing, closed landfill cells, Sunray #1 and Sunray #2 (AFIN 72-00144), were located within impact areas of the proposed Tyson Parkway interchange ramps during the project planning and design phase. Limited information was provided or could be obtained regarding the landfills. An initial interchange geometrical layout indicated the potential crossing of the two landfill cells with highway access ramps. Terracon was engaged by the project design engineer Garver, LLC (Garver) to further define and delineate the two landfill cells that would potentially be impacted by the interchange ramps construction. Terracon provided a final Geophysical Report dated July 2, 2009 that illustrated the approximate landfill limits in both the horizontal and vertical directions in the project area.

Terracon performed complementary geophysical techniques to delineate the waste mass. The geophysical survey lines and boring locations were established and documented by using GPS methods. The locations were recorded in State Plane coordinates. Lateral limits of the landfill were determined by an electromagnetic conductivity survey utilizing an EM-31 transmitting and receiving system. Electrical resistivity surface geophysical methods coupled with induced polarization (IP) methods were used to develop electrical imaging of the horizontal and vertical extent of waste.

An intrusive subsurface exploration and sampling program was developed and performed to correlate and verify the landfill delineation using “ground truth” borings. The program included four temporary monitoring wells, two per landfill, to monitor groundwater levels and to obtain groundwater samples for analytical laboratory testing. **FIGURE 1**, **FIGURE 2**, and **FIGURE 20** of the Landfill Waste Delineation project are presented at the beginning of **APPENDIX B**. **FIGURE 1** presents the preliminary interchange layout and the approximate landfill areas that were studied in the Landfill Waste Delineation project. **FIGURE 2** illustrates the study areas of interest during the delineation project. **FIGURE 20** presents the approximate waste boundaries resulting from the combined waste delineation methods.

The finalized interchange project design entailed one crossing over the Sunray #1 Landfill (western cell) A dynamic deep compaction (DDC) technique combined with constructed stone columns was used within the area of the interchange ramp that crossed the landfill. The March 2012 Work Plan was prepared to indicate the methods that were to be used to replace the low permeability soil cover of the landfill after site preparation for the roadway construction. The Work Plan presented in **APPENDIX B**, and subsequent amendments to the plan, were followed for the cover replacement in the landfill crossing.

**FIGURE 2** in **APPENDIX A** presents the as-built topographic map and layout of the Don Tyson Parkway Interchange landfill crossing project area. The Figure also shows the approximate delineated limits of the closed Sunray #1 landfill that lies south of the interchange and west of I-540 in the project area. The area which received compacted clay cover reconstruction was approximately 100 feet by 300 feet.

### 1.3 Project Description

This project involved the construction of approximately 0.7 acres of the clay barrier portion of the final cover system for this landfill. The following information summarizes the construction sequence associated with the construction of the Don Tyson Interchange.

- Site preparation including DDC, fill to subgrade, and grading of area;
- Installation and quality assurance testing of a 18-inch thick CCC, placed at a minimum of 90% of the Standard Proctor density with a maximum hydraulic conductivity of  $1.0 \times 10^{-7}$  cm/s;

The CQA Report is organized using tables, figures, and appendices to provide documentation of the observations and material testing during the construction of the final cover system for the Don Tyson Parkway Interchange.

As required by Reg.22.428(i) the CQA Report includes record drawings of the project area, and appendices and figures that identify the following:

***The limits of liner or final cover barrier construction;***

**FIGURE 2** in **APPENDIX A** depicts the limits of the DDC area and constructed final cover system for the project.

***Compaction and permeability testing locations;***

Field logs, **FIGURE 3** in **APPENDIX A**, **APPENDIX F** and **APPENDIX G** provide compaction and permeability test locations and results for the final cover system.

***In addition, the certifying professional shall make a statement that the cell was constructed in accordance with the permit drawings and narrative. The report should also include a list of any deviations from the permitted drawings, if they exist, and reasons for the deviations.***

The compacted clay cover was constructed as close as possible and in accordance with the approved Work Plan except as indicated in **SECTION 5.0** below.

### 1.4 Key Personnel

Emory Sapp & Sons, Inc. was the general contractor who performed the earthwork for the installation of the final cover and the other improvements at the site. The key personnel for each participating firm in the project are listed below.

- **CQA Consultant:**  
Terracon Consultants, Inc.
  - Certifying Engineer: F. Owen Carpenter, P.E., P.G.
  - CQA Monitor: Stephen Billingsley
  
- **Soils Contractor:**  
Emory Sapp & Sons, Inc.
  - Construction Manager: David Tag, P.E.
  
- **Soil Testing Laboratory:**  
Terracon Consultants, Inc. (Cincinnati, OH)
  - Lab Manager: Tim Goodall
  
- **Survey Control:**  
Garver
  - Project Manager: Jeff Webb, P.E.

## **2.0 SUBGRADE PREPARATION**

This section summarizes the preparation and establishment of the subgrade surface corresponding to the design for the project. The subgrade elevations conform to the approved construction drawings.

### **2.1 Project Specifications**

The approved Work Plan for the landfill cover construction (see **APPENDIX B**) called for Dynamic Deep Compaction (DDC) as the landfill improvement method for the crossing over the former Sunray #1 sanitary landfill. The DDC incorporated aspects of a variant of DDC, termed Dynamic Replacement, by creating deep columns of compacted crushed stone (“stone columns”) below the proposed ramp. A geo-grid reinforced aggregate pad was then constructed above the DDC treated area to act as a load transfer platform to distribute load to the stone columns and further reduce potential differential settlements. This provided a structurally sound platform for placement of the low permeability soil cover.

Following the DDC improvements and construction of the aggregate pad, the subgrade surface was graded, compacted, and tested to ensure that a suitable foundation for landfill cover and roadway materials was established. Quality control of the foundation (subgrade) elements was provided by the Terracon Tulsa, Oklahoma office under separate contract.

### **2.2 Construction Period**

The subgrade preparation and fill for placement of the low permeability soil cover occurred during September and October of 2013.

### **3.0 FINAL COVER PREPARATION**

This section summarizes the establishment of the compacted clay final cover barrier layer corresponding to the Sunray #1 Landfill crossing. The area was constructed as indicated in the Work Plan, for the establishment of the final cover system.

#### **3.1 Project Specifications**

The Work Plan specifications called for the final cover to be established to the lines and grades shown on the project construction plans and to consist of a minimum of 18 inches of low permeability soil compacted in lifts.

#### **3.2 Construction Procedures**

The preparation and construction for placement of the compacted clay barrier associated with the cover system occurred during September and October of 2013. The established elevations associated with the final cover system are provided in **FIGURE 2** in **APPENDIX A**.

## 4.0 LOW PERMEABILITY SOIL COVER SYSTEM INSTALLATION

The following section describes the construction of the compacted clay cover (CCC). The CCC corresponding to the project was constructed during October 2013 and was amended during March 2014 in accordance with **SECTION 5.0** below.

### 4.1 Project Specifications

The project construction plans indicated the CCC was to be constructed in three 6-inch thick compacted lifts to form a minimum 18-inch thick re-compacted clay barrier. Each clay lift was to be placed and compacted to a minimum 95% of the Standard Proctor maximum dry density at or above the optimum moisture content for the clay material. As required in the Work Plan and ADEQ Regulation 22, the hydraulic conductivity of the clay was not to exceed  $1.0 \times 10^{-7}$  cm/s.

### 4.2 Construction Procedures

Placement of the clay cover material was accomplished using excavators, 30 cubic yard haul trucks, dozers (including a dozer equipped with a sheepsfoot drum), a sheepsfoot compactor, a motor grader for proper lift thickness, and a water truck. The clay barrier was moisture conditioned during placement to achieve acceptable emplacement conditions. Dozers and the motor grader graded each lift, and compaction was achieved by utilizing a sheepsfoot compactor. Finish grading of the surface was accomplished by utilizing a total station survey and surveyor. The as-built drawing provided in **APPENDIX A** provides the final elevations associated with the top of the clay barrier for the final cover system.

### 4.3 Pre-Construction Testing of Clay Cover Material

Field and laboratory testing of the clay barrier system material was completed as specified in the ADEQ Regulation 22. Before placement, and during construction, soil samples were obtained from candidate clay stockpiles. **APPENDIX D** contains the results of the compacted clay cover pre-construction testing for the selected borrow source. **TABLE 1** summarizes the results of the pre-construction testing. It was noted during pre-construction testing of the selected clay (Cobblestone North Stockpile) that the moisture content requirement was a minimum of 2% wet of optimum moisture content at standard compactive effort. Acceptable permeability was confirmed in the lab for specimens compacted at least two percent wet of optimum at standard compactive effort (See **TABLE 1** below).

**Table 1. Clay Cover Materials Pre-Construction Test Summary**

Test Description	Moisture/Density Relationships ASTM D698	Atterberg Limits ASTM D4318	Particle Size Analysis ASTM D1140, D422	Soils Classification (USCS)	Permeability (cm/sec) D5084
<b>Project Requirements</b>	Minimum 95% Standard Proctor maximum dry density	P.I. greater than 10	> 30% passing No. 200 sieve < 20% retained No. 4 sieve No Particles >1-in diameter	SC, CL, or CH	1.0X10 <sup>-7</sup>
Sample Number			Test Results		
Cobblestone North Stockpile (10.21.13)	Max Dry Density: 110.2 pcf Optimum Moisture: 14.0%	L.L. 32 P.L. 16 P.I. 16	88.5% passing No. 200 Sieve 3.2% retained No. 4 sieve	CL	8.1X10 <sup>-7</sup>
Cobblestone North Stockpile (10.28.13 retest)	Max Dry Density: 110.2 pcf Optimum Moisture: 14.0%	L.L. 32 P.L. 16 P.I. 16	88.5% passing No. 200 Sieve 3.2% retained No. 4 sieve	CL	8.8X10 <sup>-8</sup>

#### 4.4 Construction Testing of Compacted Clay Cover Material

During the construction of the compacted cover clay barrier, samples were obtained for laboratory testing to verify the consistency of the materials during construction. The results of the construction laboratory testing are included in **APPENDIX E. TABLE 2** summarizes the results obtained from laboratory testing of the CCC material. Based upon the results of the construction testing performed, all of the clay cover material complied with the project specifications. After placement and verification of the clay cover material, the clay cover in the roadway alignment was amended in accordance with **SECTION 5.0** below. Compaction characteristics of the lime treated soils discussed in **SECTION 5.0** are presented in **TABLE 2** below.



**Table 2. Compacted Clay Cover Materials Construction Test Summary**

Test Description	Moisture/Density Relationships ASTM D698	Atterberg Limits ASTM D4318	Particle Size Analysis ASTM D1140, D422	Soils Classification (USCS)	Permeability (cm/sec) D5084
<b>Project Requirements</b>	Minimum 95% Standard Proctor maximum dry density	P.I. greater than 10	> 30% passing No. 200 sieve <20% retained No. 4 sieve No Particles >1-in diameter	SC, CL, or CH	1.0X10 <sup>-7</sup>
<b>Sample Number</b>	<b>Test Results</b>				
Bulk #2 Cobblestone North Stockpile	Max Dry Density: 108.3 pcf Optimum Moisture: 16.3%	L.L 31 P.L.17 P.I. 14	59.3% passing No. 200 Sieve 17.2% retained No. 4 Sieve	CL	1.2X10 <sup>-8</sup>
Lime Treated Cobblestone North Stockpile	Max Dry Density: 105.5 pcf Optimum Moisture: 18.3%				

Field moisture and density tests were planned to be performed at a minimum rate of one test for every 10,000 square feet per compacted lift of newly emplaced cover system clay barrier soil. **FIGURE 3** illustrates the locations of the field moisture and density tests for each compacted lift of new clay cover. **APPENDIX F** includes the field logs for the moisture and density testing performed in association with the CCC construction. Based upon the results of the moisture and density tests performed by Terracon, the three lifts of compacted clay cover comply with the project specifications.

Shelby tube samples were obtained from each lift at a minimum rate of one test for every 40,000 square feet. **FIGURE 3** illustrates the permeability testing locations where the Shelby Tube samples were taken for each compacted lift of clay. The tubes were sealed and delivered to the laboratory for permeability testing using a flexible-wall permeameter (ASTM D-5084). As indicated in **TABLE 3**, permeability results for the completed compacted clay cover met the project requirements (less than  $1 \times 10^{-7}$  cm/s from Reg. 22.428). **APPENDIX G** contains the compacted clay cover permeability test results.

**Table 3 Permeability Results Summary**

Test No.	Lift No./ Layer	Test Results	
		K (cm/sec)	Pass/ Fail
P-1	1/CCC	$3.9 \times 10^{-8}$	Pass
P-2	2/CCC	$3.0 \times 10^{-8}$	Pass
P-3	3/CCC	$4.9 \times 10^{-8}$	Pass
P-4	3/CCC	$3.5 \times 10^{-8}$	Pass

NOTE: CCC = Compacted Clay Cover, K = Hydraulic Conductivity

## 5.0 CONSTRUCTION MODIFICATIONS

CCC clay soils were constructed with in-place moisture content wet of optimum moisture content as described in **SECTION 4.3**. Subsequent to emplacement and testing of the CCC clay soils, it was determined that the relatively moist soils exhibited unacceptable pumping conditions with respect to providing an adequate roadway structural subgrade. Therefore, the clay soils were amended with 6% lime dust by weight and re-compacted to a minimum density of 95% of the Standard Proctor maximum dry density at a moisture content of plus or minus two percent of optimum moisture content for the lime amended soils. **APPENDIX F** includes the field logs for the moisture and density testing performed on the lime amended clay barrier soils.

Correspondence related to the amended and replaced soils is presented in **APPENDIX B**. The lime amended soils are expected to exhibit slow permeabilities and act as an infiltration barrier as demonstrated by testing of the initial placement of the barrier soils as documented above. The amended soils in the roadway area were also to receive hard armoring in the form of asphalt paving which will increase the capacity of the roadway section to limit infiltration into the underlying landfill.

The pavement will exhibit enhanced run-off when compared to soils in the assignment of curve numbers for soils versus pavement in TR-55 software. Pavement is assigned a curve number of 98 corresponding to run-off in TR-55 software. The highest available curve number within the TR-55 run-off modeling software for a soil in Hydrologic Soil Group D (includes clay used for the CCC) is 94. Therefore it is expected that the hard armoring within the roadway will more efficiently limit infiltration into the landfill than the barrier soils.

## **6.0 SUMMARY**

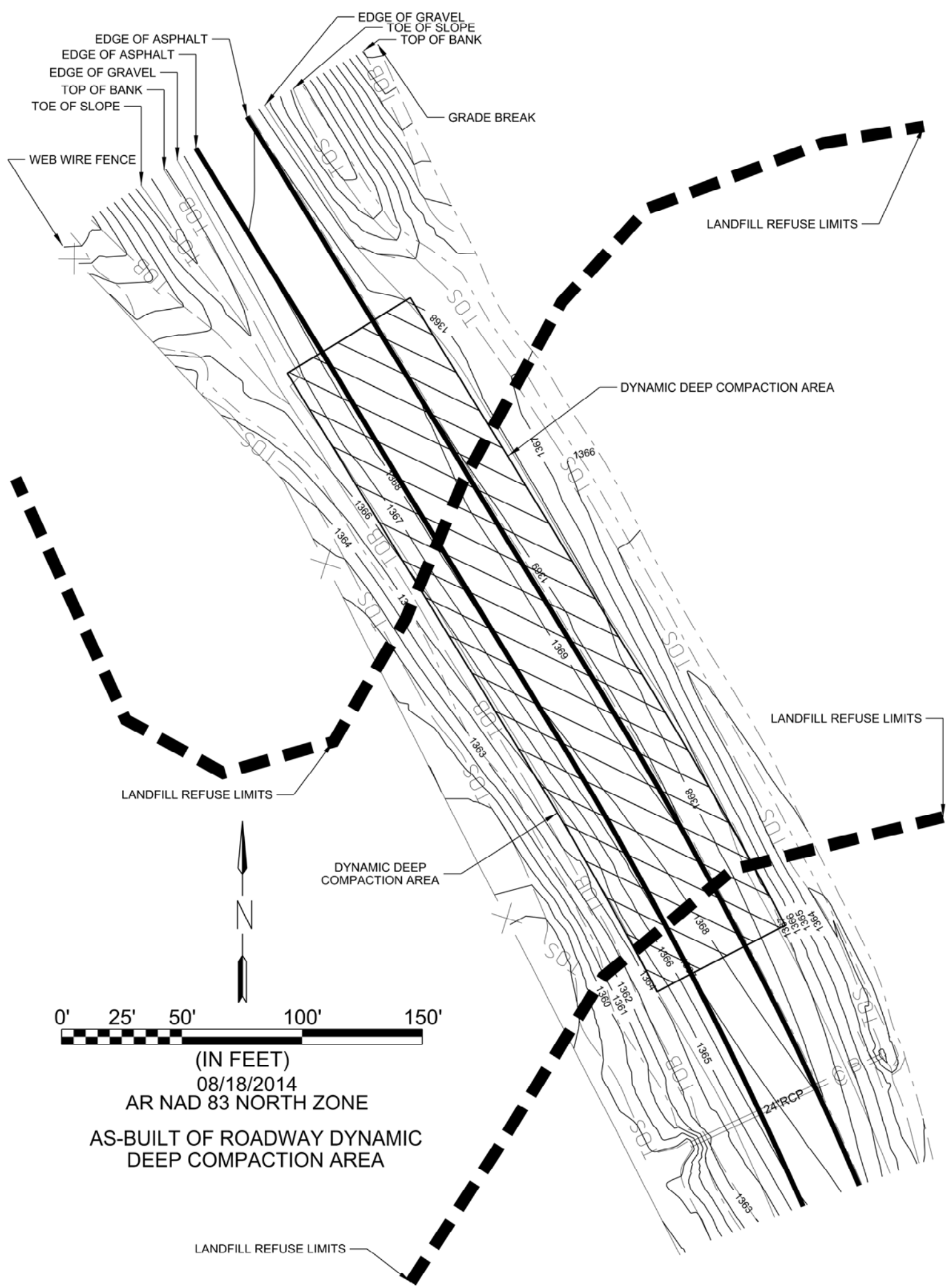
Terracon was retained by Garver, LLC to provide construction quality control services during the construction of the compacted clay cover reconstruction for the Sunray Landfill. The lines, grades, thickness, and elevations of the CCC were documented and certified by Garver, LLC. Survey data is available upon request.

The quality control program conducted by Terracon included: pre-construction sampling of soils; observation, sampling, and testing of construction and materials. Laboratory testing of the materials was conducted by Terracon Consultants, Inc. in Cincinnati, OH.

The observations made by and the results of tests conducted by Terracon and the referenced laboratory indicate that the compacted clay barrier portion of the final cover in the affected areas of the Sunray Landfill was constructed in compliance with the documents referenced in this report except as documented in **SECTION 5.0**.

# **Appendix A**

## As-Built Drawings



REV.	DATE	BY	DESCRIPTION

**Terracon**  
 Consulting Engineers and Scientists

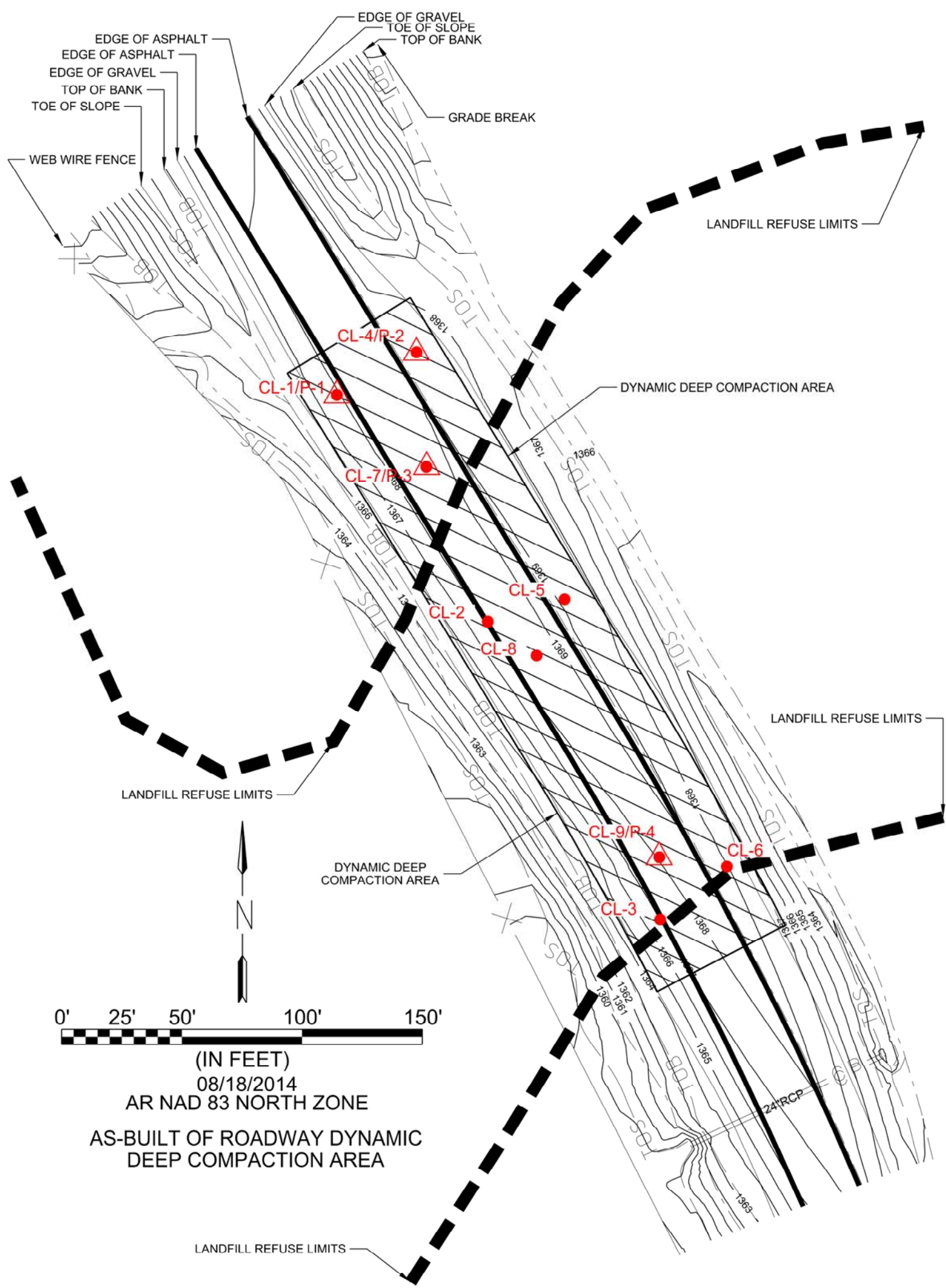
11400 WEST BASELINE ROAD LITTLE ROCK, AR 72209  
 PH. (501) 455-2199 FAX. (501) 455-4547

**AS-BUILT**  
 DON TYSON PARKWAY  
**GARVER**  
 HIGHWAY INTERCHANGE LANDFILL CROSSING  
 SPRINGDALE ARKANSAS

**FIGURE 1**

DESIGNED BY:	JSB
DRAWN BY:	JSB
APPVD. BY:	FOC
SCALE:	1"=50'
DATE:	09/15/2014
JOB NO.:	544-001-35139161
ACAD NO.:	001
SHEET NO.:	1 OF 2





(IN FEET)  
 08/18/2014  
 AR NAD 83 NORTH ZONE  
 AS-BUILT OF ROADWAY DYNAMIC  
 DEEP COMPACTION AREA

- LEGEND**
- CL-1 ● TEST LOCATION
  - P-1 ▲ PERMEABILITY SAMPLE LOCATION

REV.	DATE	BY	DESCRIPTION

**Terracon**  
 Consulting Engineers and Scientists

11400 WEST BASELINE ROAD      LITTLE ROCK, AR 72209  
 PH. (501) 455-2199      FAX. (501) 455-4547

**TEST LOCATION MAP**  
 DON TYSON PARKWAY  
**GARVER**  
 HIGHWAY INTERCHANGE LANDFILL CROSSING  
 SPRINGDALE      ARKANSAS

**FIGURE 2**

DESIGNED BY:	JSB
DRAWN BY:	JSB
APPVD. BY:	FOC
SCALE:	1"=50'
DATE:	09/15/2014
JOB NO.:	544-001-35139161
ACAD NO.:	002
SHEET NO.:	2 OF 2

## **Appendix B**

### General Project Correspondence



# Terracon

Consulting Engineers & Scientists

July 2, 2009

Garver Engineers, LLC  
1088 East Millsap Road  
Fayetteville, Arkansas 72703

Terracon Consultants, Inc.  
25809 I-30  
Bryant, Arkansas 72022  
Phone 501.847.9292  
Fax 501.847.9210

Attention: Ms. Natalie Becknell, P.E.

Re: Geophysical Report  
Landfill Waste Delineation  
Don Tyson Parkway Interchange  
Springdale, Arkansas  
Project No. 39085057

Dear Ms. Becknell,

We are submitting, herewith, the results of the subsurface exploration and forensic consulting services performed for the Don Tyson Parkway Interchange landfill delineation project in Springdale, Arkansas. The geophysical subsurface exploration was completed as outlined in Terracon Proposal No. P3908032, authorized on October 31, 2008.

We appreciate the opportunity to be of service to you on this project. If you have any questions, we would be pleased to discuss our findings and recommendations in greater detail with you.

Sincerely,

**Terracon**

Certificate of Authorization #223, Expires 12/31/09  
ARKANSAS

\*\*\* 7/2/2009

REGISTERED  
PROFESSIONAL  
SHAUN P. BAKER, P.E.

Arkansas No. 11817

No. 11817

SHAUN P. BAKER

SPB:FOC:DWM

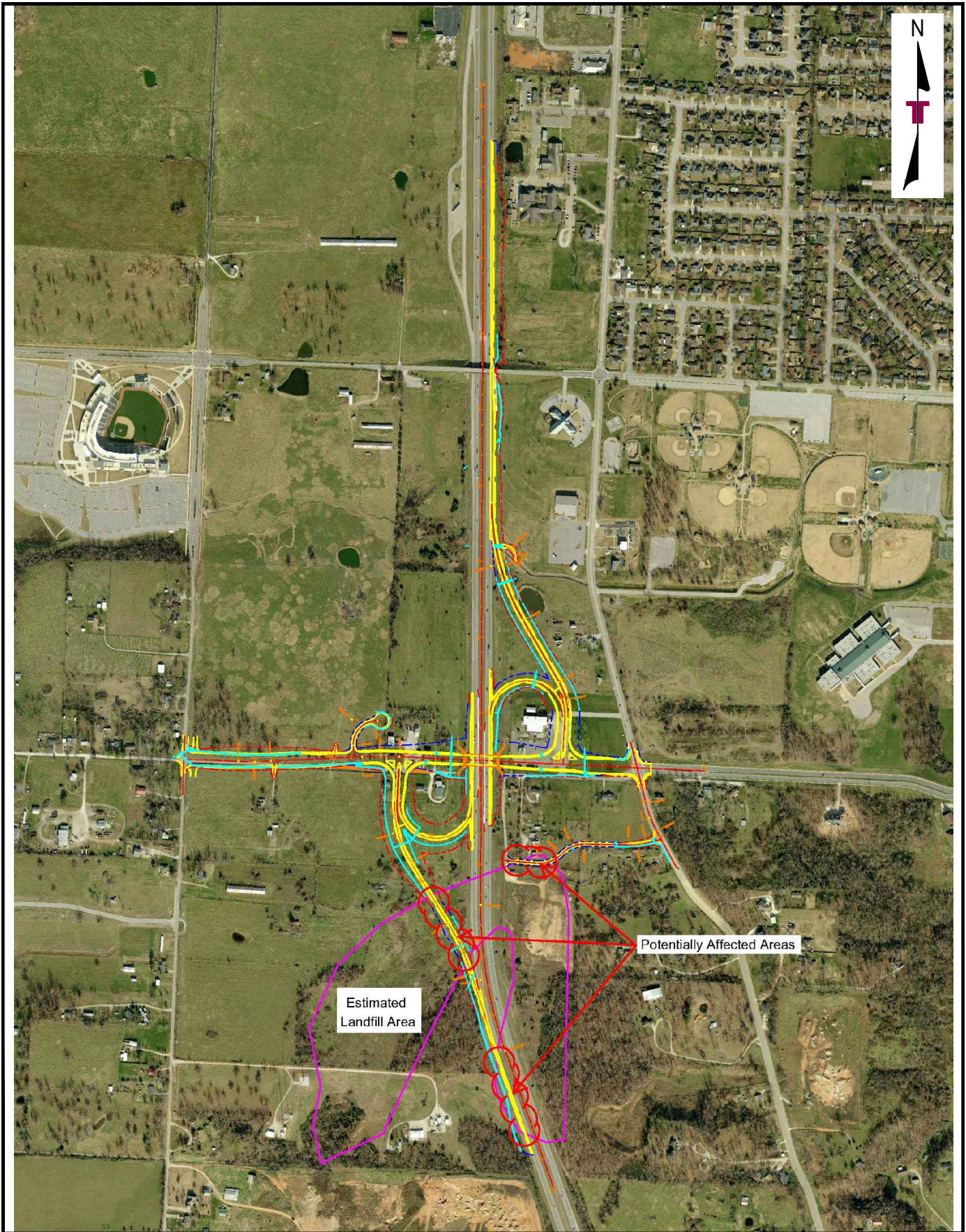
Enclosures



Daniel W. McCullough, P.G.  
Arkansas No. 1802

Copies to: Addressee (3+e-mail)





Project Mng: DCM  
Drawn By: PTG  
Checked By: DCM  
Approved By: DCM

Project No. 167-024-39085057  
Scale: N.T.S.  
File No. 024  
Date: 3/27/2012

**Terracon**  
Consulting Engineers and Scientists

25809 I-30 SOUTH BRYANT, AR 72022  
PH. (501) 847-9292 FAX. (501) 847-9210

GENERAL SITE LAYOUT  
GARVER ENGINEERS, LLC.  
TYSON PARKWAY INTERCHANGE  
SPRINGDALE ARKANSAS

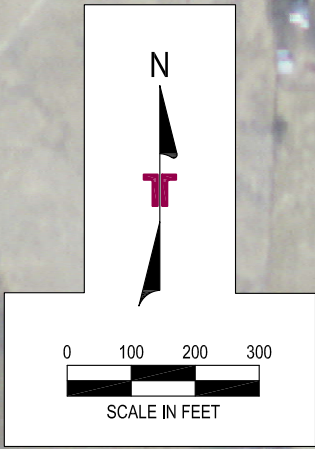
FIG. No.  
1







COMBINED RESULTS OF WASTE BOUNDARY SURVEYS  
 TYSON INTERCHANGE - SPRINGDALE, ARKANSAS





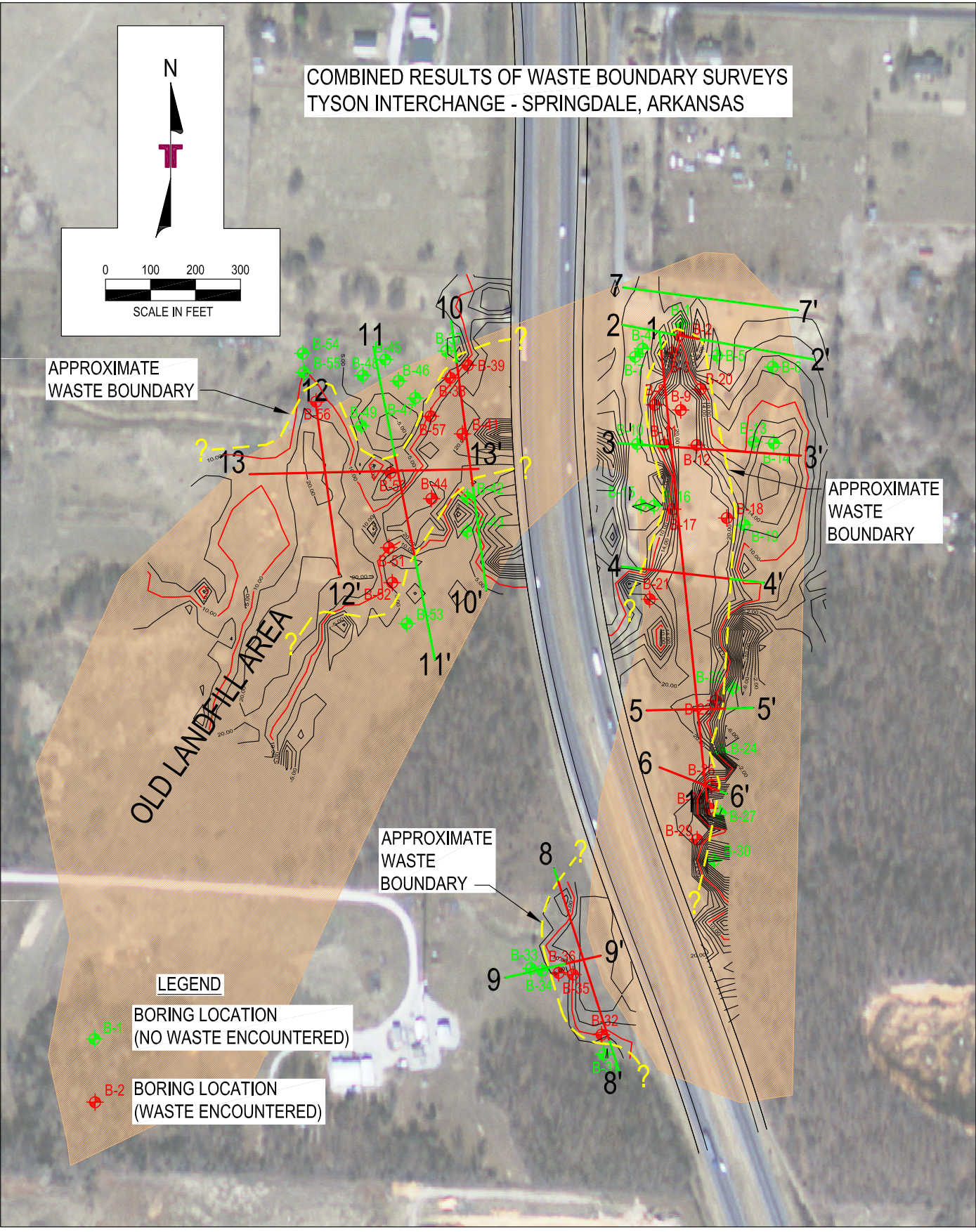
APPROXIMATE  
 WASTE BOUNDARY

APPROXIMATE  
 WASTE BOUNDARY

OLD LANDFILL AREA

LEGEND

-  B-1 BORING LOCATION (NO WASTE ENCOUNTERED)
-  B-2 BORING LOCATION (WASTE ENCOUNTERED)



Project Mng'r:	SPB
Drawn By:	JEG
Checked By:	TSW
Approved By:	SPB

Project No.	167-024-39085057
Scale:	AS SHOWN
File No.	022
Date:	06/18/2009

**Terracon**  
 Consulting Engineers and Scientists

25809 I-30 SOUTH BRYANT, AR 72022  
 PH. (501) 847-9292 FAX. (501) 847-9210

APPROXIMATE WASTE BOUNDARY  
 LANDFILL WASTE DELINEATION  
**GARVER ENGINEERS, LLC.**  
 TYSON PARKWAY INTERCHANGE  
 SPRINGDALE ARKANSAS

FIG. No.	20
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# WORK PLAN

## Don Tyson Parkway Interchange Springdale, Arkansas

March 29, 2012  
Project No. 35117167

### Prepared for:

Garver, LLC  
1088 East Milsap Road  
Fayetteville, Arkansas 72703

### Prepared by:

Terracon Consultants, Inc.  
Little Rock, Arkansas

Offices Nationwide  
Employee-Owned

Established in 1965  
[terracon.com](http://terracon.com)

# Terracon

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## WORK PLAN

### DON TYSON PARKWAY INTERCHANGE SPRINGDALE, ARKANSAS

Project No. 35117167

March 29, 2012

## INTRODUCTION

We understand that the project will include an extension of Don Tyson Parkway beginning at the intersection of Don Tyson Parkway and 48<sup>th</sup> Street, then extending to 56<sup>th</sup> Street. The extension of Don Tyson Parkway will include reconstruction (widening) and renaming of West Oaklawn Drive and Dearing Road and include a new interchange at Interstate 540. The proposed project will also include an extension of 56<sup>th</sup> Street from recent improvements at Arvest Ballpark to, and including, a new intersection at 56<sup>th</sup> Street and Don Tyson Parkway. The proposed project will provide a 4-lane or 5-lane facility on Don Tyson Parkway and 56<sup>th</sup> Street through the project limits, with medians, where feasible, and curb and gutter and sidewalks on both sides of the roadway. Storm drainage systems, new and relocated utility facilities, traffic signals, street lighting, and other incidental systems and facilities will be constructed as necessary. The project will be constructed both along existing roadways and in new locations. A portion of the project will be constructed above closed landfills as described below. Construction will be on right of way acquired by the City of Springdale, Arkansas and on Arkansas Highway and Transportation (AHTD) right of way.

## PROJECT SITE HISTORY

Two landfills, Sunray #1 and Sunray #2, are located in areas of the proposed Tyson Parkway interchange ramps. Limited information was provided or could be obtained regarding the landfills. **Figure 1** shows the approximate extent of the landfill waste relative to Interstate 540. **Figure 1** shows the proposed Tyson Parkway Interchange project area with the approximate limits of the abandoned Sunray #1 and Sunray #2 landfills that lie south of the proposed interchanges, stretching across I-540 and under the proposed ramps.

Sunray #1 landfill was permitted to begin operations in December 1973. The closure date could not be determined. The Sunray #2 landfill was permitted to begin operations in February 1977 and continued through November 1978. A generally north-south oriented ravine was filled from north to south with municipal solid waste for both the Sunray # 1 and Sunray # 2 landfills. Industrial and/or hazardous wastes were not permitted for disposal in the landfills.

## ROAD SUBGRADE IMPROVEMENT METHODS

It is estimated that an approximately 200 to 300 feet of the proposed Ramp 4 will be constructed over buried landfill waste. Based on borings drilled previously by Terracon, landfill waste was encountered at depths of about 2 to 5.5 feet below the existing ground surface. The waste extends to depths of about 6 to 23 feet. We also understand that up to 5 feet of embankment fill will be required to reach the final pavement grade within that section.

The proposed landfill improvement method for the crossing over the former Sunray #1 sanitary landfill is Dynamic Deep Compaction (DDC) incorporating aspects of a variant of DDC, sometimes termed Dynamic Replacement, with the intention of creating deep columns of compacted crushed stone ("stone columns") below the proposed ramp. A geo-grid reinforced aggregate pad is proposed to be constructed above the DDC treated area to act as a load transfer platform to distribute load to the stone columns and further reduce potential differential settlements. A conceptual cross section of the ramp, incorporating the proposed ground improvement measures, is provided by the attached **Figure 2**. The DDC method was used to treat a larger area of the Sunray #1 and #2 landfills during previous construction of U. S. Rte. 71/I-540 in the mid-1980s.

### Dynamic deep compaction (DDC)

Dynamic compaction consists of using a heavy tamper that is repeatedly raised and dropped from varying heights to impact the ground. The mass of the tampers generally ranges from about 5 to 30 tons and drop heights range from about 40 to 100 feet. Lighter tampers and smaller drop heights result in depths of improvement on the order of about 10 to 15 feet and heavier tampers and greater drop heights result in improvements on the order of 20 to 30 feet.

The proposed roadway (travel lanes plus paved shoulders) is indicated to be 25 feet wide on a 60-foot wide embankment. Assuming that the primary concern is with the paved roadway, we have tentatively assumed a width to be treated that is effectively 48 to 60 feet wide or roughly twice the width of the roadway (see **Figures 2 & 3**).

### Stone columns

Stone columns are vertical piers of compacted crushed stone that act to carry loads through zones of loose or compressible soil and/or waste. Construction of stone columns also typically results in densification of the loose or unsuitable soil. A form of "stone column" can be created in conjunction with dynamic compaction process by filling the craters resulting from dropping the weight with crushed stone after each drop. The stone columns will improve the transmission of energy to greater depths than would otherwise occur with conventional dynamic compaction. The stone columns will also form a strong skeleton in the landfill waste, and therefore reduce the potential for the long-term settlement due to further decay and decomposition of the landfill waste (See **Figure 2**).



## **Geogrid reinforced aggregate mat**

Geogrid reinforced aggregate mats consist of alternate layers of geogrid and crushed aggregate base materials. Construction of a layer of geogrid reinforced aggregate mat is intended to distribute stress over a larger area and reduce differential settlement. Geogrid reinforced aggregate mats are used both for roadway construction across soft subgrades and as a load transfer platform used with an intermediate foundation system, such as Geopiers or stone columns.

The combination of dynamic compaction, stone columns and geogrid reinforced aggregate mats will reduce both short-term and long-term settlement. A more detailed description of the site preparation above the landfills are discussed below.

# **LANDFILL AREA PREPARATION**

## **Site Preparation**

The grading of the working surface for the DDC work will need to be coordinated with the ramp design so that the horizontal and vertical alignment can be accommodated. There is an existing final cover of 2 to 3 feet of clayey soil over the waste that is assumed to act as the landfill cap. As the DDC process will disrupt this “cap” and render it ineffective, this soil can be removed as necessary to establish the appropriate geometry for ramp construction. However, grading that exposes the waste below the existing cover should be avoided. If waste is exposed, it should be covered with the crushed stone working mat (see below) on the same day it is exposed, consistent with sanitary landfill operating practices. Also, any excess waste will be required to be removed and disposed in an approved Subtitle D landfill. The surrounding work area will be graded such that rain drains away from the work area. If there is a possibility of rain, the work area will be covered with at least 6-inches of temporary soil or a tarp in order to keep moisture out of the waste area. Any liquids encountered that have come in contact with the waste will be treated as leachate and disposed of at a permitted facility.

Once the desired preparation grades are achieved, the DDC work area should be covered with 18 to 24 inches of crushed stone as a working mat.

## **Crushed Stone**

Most any “clean” (less than 5 percent fines) durable granular material (to include crushed concrete and masonry rubble) can be used in conjunction with the DDC process. It is expected that a crushed stone quarry product would be used as was used

in the original I-540 construction. The specification for the previous DDC work was crushed limestone or dolomite with a maximum stone size of 6 inches, no more than 15% passing 1.5-inch and no more than 5% passing ¾-inch. The same type of materials will be used or equivalent as deemed by the Project Engineer.

### **DDC Process**

As described above, dynamic deep compaction (DDC) is a process whereby a heavy weight (called a “pounder” or “tamper”) is repeatedly raised and dropped from a specified height to impact onto the ground surface, thereby transmitting high compaction energy into the soil mass. The depth of the improvement depends upon the amount of energy and the height of the fall. The degree of the improvement depends upon the amount of energy applied per unit area which also takes into consideration the number of passes over the work area and the number of times the weight is dropped at each location. For the dynamic replacement variant of DDC, the crater resulting from the pounder impact is backfilled with granular material after each drop, with the intention of driving the backfill into the ground to displace the loose or unsuitable material and create a vertical column of compacted granular material. The displacement of existing soil from the column results in densification of the surrounding soil. The preliminary drop point pattern and sequence of treatment is shown in **Figure 3**.

The DDC/dynamic replacement work sequence is envisioned as follows:

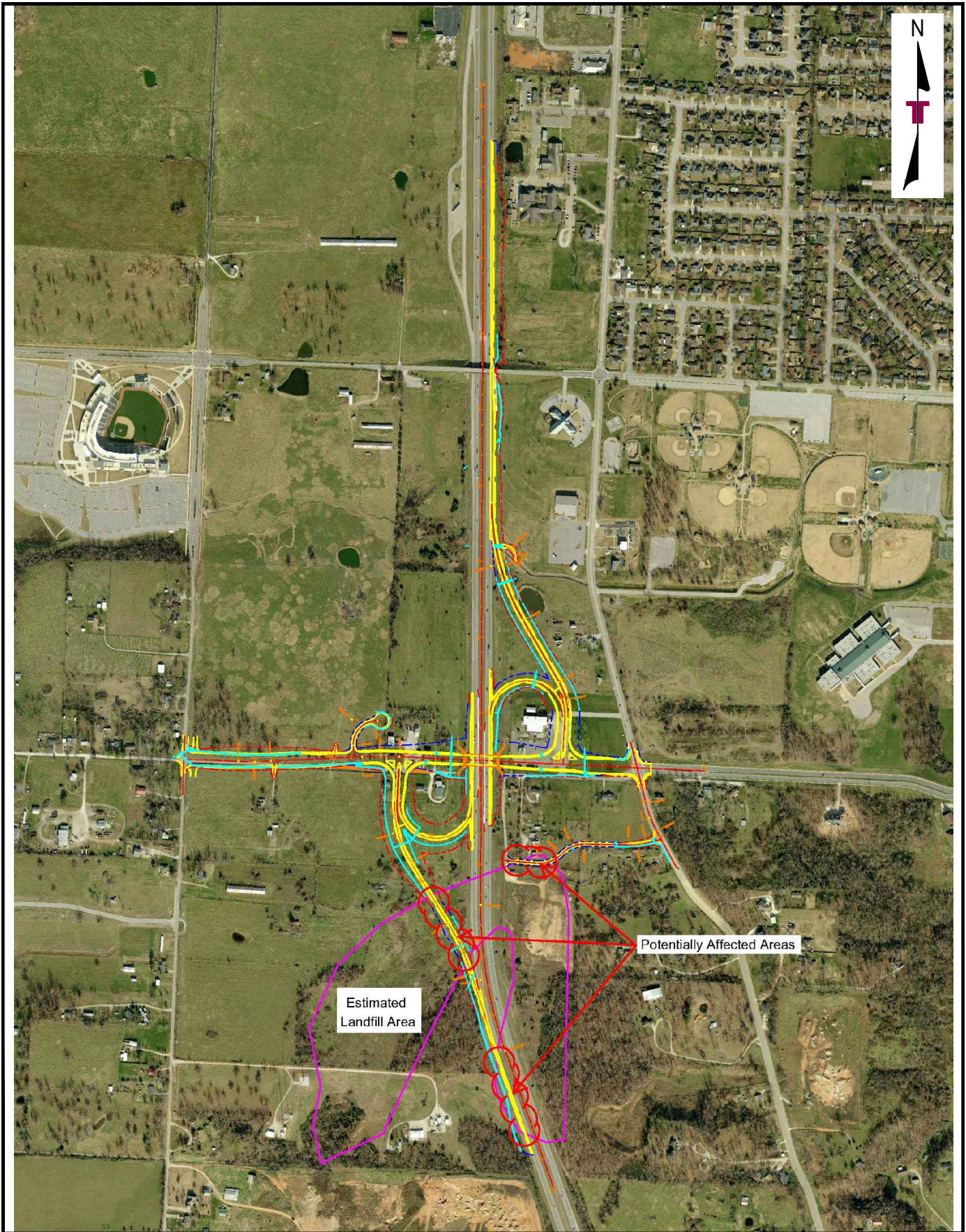
1. Clear, grub, strip and grade to desired preparation grading. Place working mat of 18 to 24 inches of crushed stone.
2. Layout drop points for primary pass.
3. Start on ramp centerline at center of area to be treated. Drop pounder to create crater. After each drop, backfill crater with crushed stone. Continue until the incremental ground surface displacement totals less than six inches after two consecutive drops. Eight to twelve drops per location are expected in areas underlain by waste. Maintain records of ground displacement (crater depths) after each drop and the volume of crushed stone added as backfill.
4. Repeat the foregoing drop/backfill process at each primary drop point in the sequence indicated on Exhibit A-2.
5. Regrade the work area surface after completion of the primary pass. Layout secondary pass drop locations.

6. Perform drop/backfill procedure at each secondary drop location in sequence. The number drops per location is expected to be less than for the primary pass.
7. Perform “ironing pass”, incrementally compacting entire work area surface.
8. After “ironing pass”, grade work area surface smooth and proof compact with at least six passes of a large self-propelled vibratory drum roller with a dynamic force of at least 8,000 pounds per foot of drum width. Perform elevation survey of surface after proof compaction.

### **Embankment Construction**

Once the DDC process is completed, construction of the embankment and roadway will proceed normally. The geo-grid reinforce aggregate mat would act as a load transfer platform to span between drop point locations and to “smooth out” potential differential settlement. The geo-grid reinforced aggregate mat concept is illustrated on **Figure 2**. Detailed design of the geo-grid reinforced aggregate mat would depend on the geometry of the embankment and expected loading. Typically it would consist of one to three layers of bi-axial or tri-axial geo-grid with each geo-grid covered by about 6 inches of compacted 3”(-) compacted aggregate. In consideration of the expected disruption of the existing landfill cover by the DDC process, **Figure 2** indicates that “embankment” material used above the landfill will consist of low permeability soil ( $1 \times 10^{-7}$  cm/sec or slower). The replacement soil liner will consist of at least 18 inches of material that meets Regulation 22 requirements for materials and testing (**See Arkansas Department of Environmental Quality (ADEQ) Regulations, Reg.22.428 – Liner and Final Cover Design and Construction**). The 18 inches of replacement soil liner will transition into the current soil cover with a 3 H: 1V tie-in. A CQA report detailing the installation of the soil liner will be submitted to the ADEQ for review.





Project Mng: DCM  
Drawn By: PTG  
Checked By: DCM  
Approved By: DCM

Project No. 167-024-39085057  
Scale: N.T.S.  
File No. 024  
Date: 3/27/2012

**Terracon**  
Consulting Engineers and Scientists

25809 I-30 SOUTH BRYANT, AR 72022  
PH. (501) 847-9292 FAX. (501) 847-9210

GENERAL SITE LAYOUT

GARVER ENGINEERS, LLC.  
TYSON PARKWAY INTERCHANGE

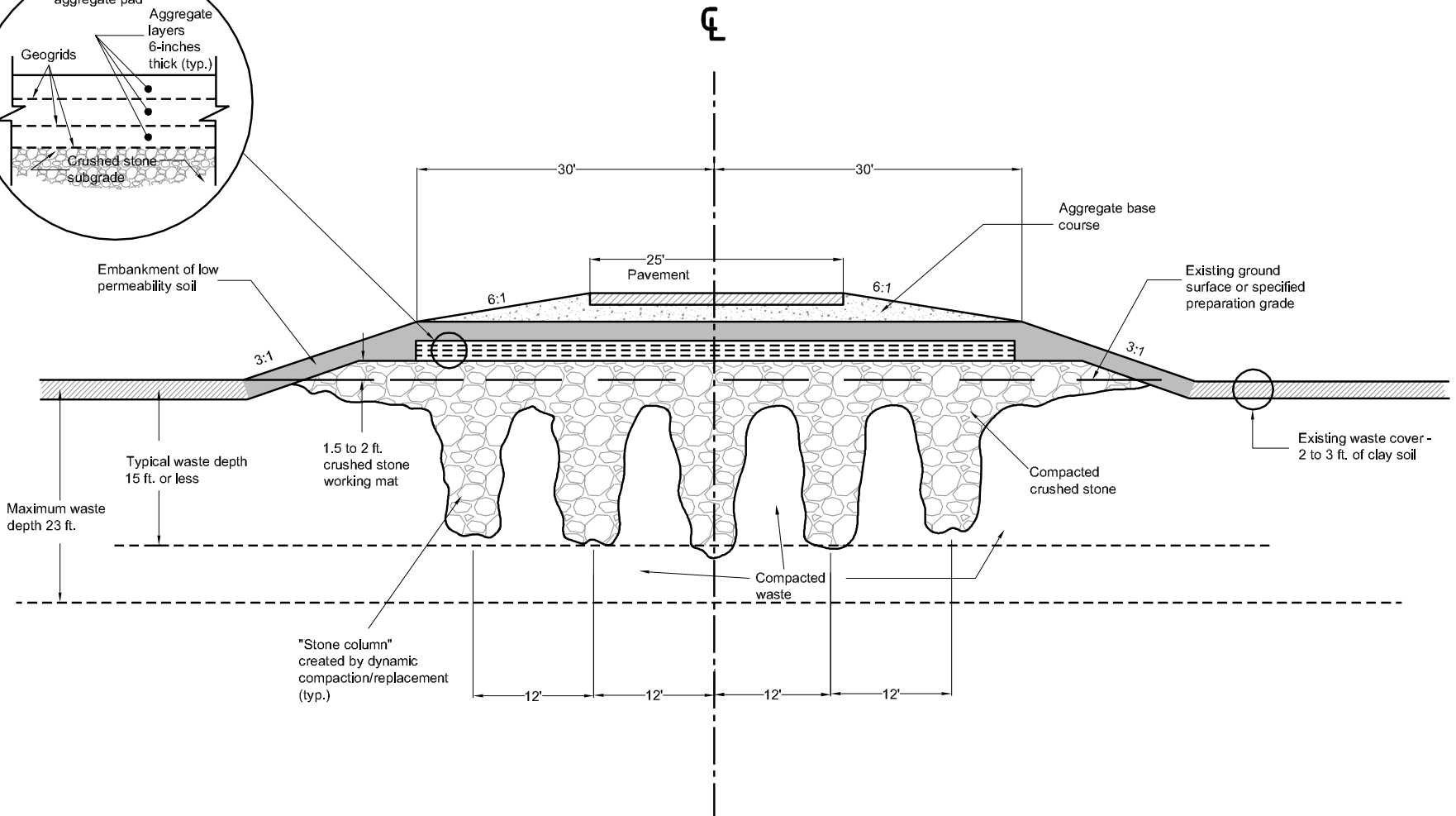
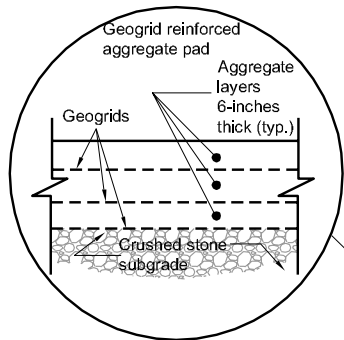
SPRINGDALE

ARKANSAS

FIG. No.

1





Project Mngr:	RMD
Drawn By:	MCR
Checked By:	RMD
Approved By:	

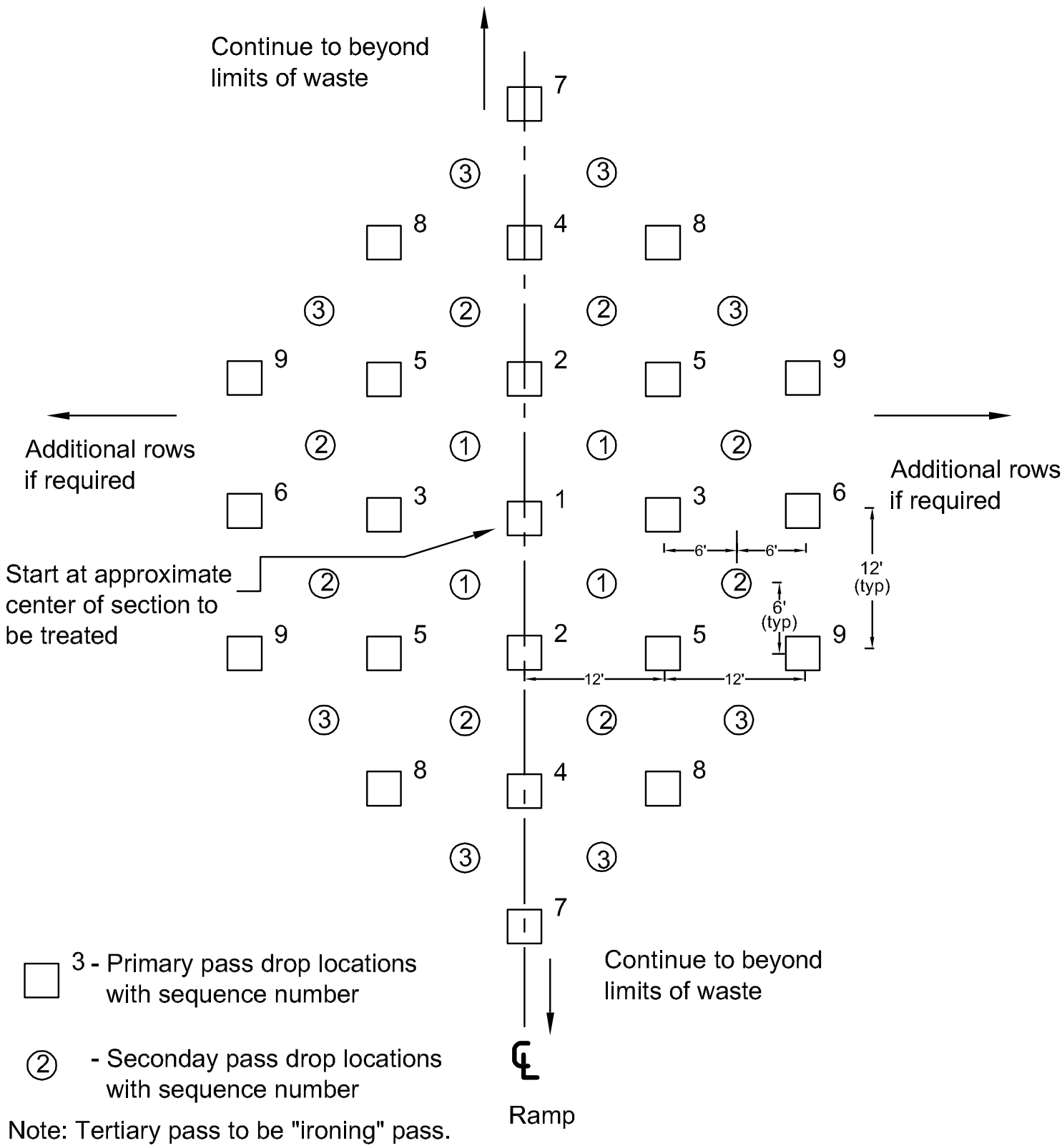
Project No.	04115042
Scale:	1" = 16'
File No.	04115042.dwg
Date:	February 2012

**Terracon**

10930 E. 58th St. Tulsa OK 74146  
 PH. 918-250-0461 FAX 918-250-4670

CONCEPTUAL RAMP CROSS-SECTION  
 AT OLD LANDFILL CROSSING  
 TYSON PARKWAY INTERCHANGE  
 SPRINGDALE, ARKANSAS

FIG. No.	2
----------	---



Project Mng:	RMD
Drawn By:	MCR
Checked By:	RMD
Approved By:	

Project No.	04115042
Scale:	1" = 12'
File No.	04115042.dwg
Date:	February 2012

**Terracon**

10930 E. 58th St. Tulsa OK 74148  
PH. 918-250-0481 FAX 918-250-4570

DDC DROP PATTERN AND SEQUENCE

TYSON PARKWAY INTERCHANGE  
SPRINGDALE, ARKANSAS

FIG. No.

3

# Memo

**TO:** Justin Cox, P.E., Mike Homan, P.E. (Terracon Tulsa Office)  
**FROM:** F. Owen Carpenter, P.E., P.G.  
**CC:** Billy Butler, P.E.  
**DATE:** Friday, January 17, 2014  
**RE:** Don Tyson Parkway Interchange, Springdale, AR  
Clay Cover Soil

---

## **Approved Cover Soil Specifications Per ADEQ Regulation 22.428**

The approved Workplan dated March 29, 2012, submitted to the Arkansas Department of Environmental Quality (ADEQ), required that the replacement soil cover will consist of 18 inches of material that meets Regulation 22 requirements for materials and testing (Reg.22.428 – Liner and Final Cover Design and Construction). Criteria are:

- Material passing #200 sieve – Greater than 30%
- USCS Classification – CL, CH or SC with PI greater than 10
- Material greater than #4 sieve less than 20% with no particles greater than 1.0 inch diameter
- Hydraulic conductivity of  $1 \times 10^{-7}$  cm/sec or less and at a minimum of 90% Standard Proctor maximum dry density at a moisture content above optimum as determined by ASTM D698

## **Cover Soil Characterization for Soils used in Cover Construction October 2013**

Potential low permeability cover soils provided by David Tag of Emery Sapp & Sons, Inc. ([David.Tag@Emerysapp.com](mailto:David.Tag@Emerysapp.com)) were tested and material characterized as Cobblewood – North Stockpile was used for clay cover construction. During pre-construction laboratory hydraulic conductivity testing at a specified compaction (ASTM D5084), required by Reg 22.428(c)(6)(v), it was concluded that specimens compacted at optimum moisture content did not exhibit acceptable hydraulic conductivity results ( $8.1 \times 10^{-7}$  cm/sec). Subsequent testing indicated that specimens compacted at a minimum of 2% wet of optimum moisture content at standard compactive effort would yield acceptable permeability results (less than or equal to  $1 \times 10^{-7}$  cm/sec). Therefore the field specification based on pre-construction testing was to emplace the cover soils using standard compactive effort at a minimum of 2% wet of optimum moisture content and a maximum range of 2% to 6% wet of optimum. Resulting verification hydraulic conductivity values were acceptable and ranged from  $3.0 \times 10^{-8}$  to  $4.9 \times 10^{-8}$  cm/sec.

N:\Projects\2013\35139161\EMAIL-OTHER COMMUNICATIONS\Memo - Clay Cover Specs.docx

Bryant, Arkansas

## Carpenter, Owen

---

**From:** Carpenter, Owen  
**Sent:** Tuesday, March 25, 2014 12:21 PM  
**To:** DJWebb@GarverUSA.com  
**Cc:** rspetrie@garverusa.com; Cox, Justin D; Butler, William P.; Leamons, Bryan (LEAMONS@adeq.state.ar.us)  
**Subject:** Don Tyson Parkway Interchange - Proctor for 6% lime stabilized clay sample  
**Attachments:** Std Proctor 6 percent lime.pdf

**Follow Up Flag:** Follow up  
**Flag Status:** Flagged

Good morning Jeff,

Please pardon the delay in getting this confirmatory email to you following our discussion this morning.

First of all, I spoke with Bryan Leamons in the Solid Waste Management Division of the ADEQ. I am copying him on this email. In light of the fact that the clay soils exhibited too much deflection even when emplaced in a relatively dry state, the contractor plans to amend the soils within the roadway section with 6% lime dust by weight and to re-compact them to a specified Proctor moisture and density. We intend to test the soils for their in-situ properties after emplacement and document the deviation within our CQA report required by the ADEQ Work Plan. A statement regarding the hydraulic efficiency of the pavement in this application in removing stormwater from the area will be added to the CQA report.

The laboratory Proctor test results are attached to this email. This is for the roadway area clay cap materials with six percent lime added by weight.

Field moisture density testing will be performed by our Tulsa office. If at all possible, please notify the Tulsa office dispatch number (918) 250-6051 at least 24 hours in advance of needed testing. If you fail to reach the dispatcher, please contact Mr. Justin Cox at (918) 948-9871.

If you have any questions or desire any additional information, please contact me at your earliest convenience. Thank you for your assistance with these matters.

Sincerely,  
Owen

**F. Owen Carpenter, P.E., P.G.**  
**Engineering Manager | Solid Waste Services**

**Terracon Consultants, Inc.**

25809 I-30 South | Bryant, Arkansas 72022

P (501) 847 9292 | F (501) 847 9210

D (501) 943 1020 | C (501) 622 0887

[focarpenter@terracon.com](mailto:focarpenter@terracon.com) | [www.terracon.com](http://www.terracon.com)



# LABORATORY COMPACTION CHARACTERISTICS OF SOIL REPORT



Report Number: 35139161.0001

Service Date: 03/24/14

Report Date: 03/24/14

25809 I-30 South  
Bryant, AR 72022  
501-847-9292

## Client

Garver  
Attn: Ron Petrie  
2049 E. Joyce Blvd. Ste 400  
Fayetteville, AR 72703-5394

## Project

Tyson Parkway Extension  
Don Tyson Parkway and Interstate 540  
Springdale, AR

Project Number 35139161

## Material Information

Source of Material: On-site Fill  
Proposed Use: Fill

## Sample Information

Sample Date: 03/21/14  
Sampled By: Gramling, Paul  
Sample Location: On-site

Sample Description: PENDING PROCTOR

## Laboratory Test Data

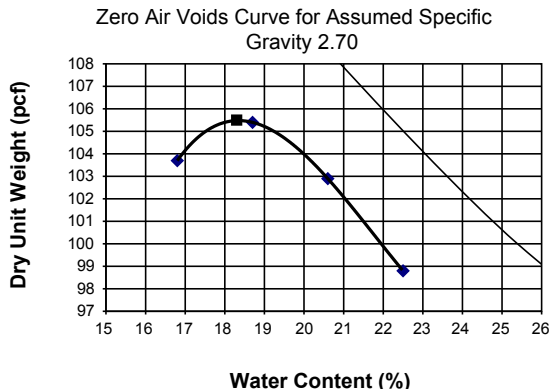
Test Procedure: ASTM D698  
Test Method: Method B  
Sample Preparation: Wet  
Rammer Type: Manual  
Maximum Dry Unit Weight (pcf): 105.5  
Optimum Water Content (%): 18.3

Liquid Limit:  
Plastic Limit:  
Plasticity Index:  
In-Place Moisture (%):

Result

Specifications

USCS:



Comments:

Services:

Terracon Rep.:

Reported To:

Contractor:

Report Distribution:

(1) Garver, Ron Petrie

Reviewed By: \_\_\_\_\_

William Butler  
Senior Staff Engineer

Test Methods: AASHTO T99

The tests were performed in general accordance with applicable ASTM, AASHTO, or DOT test methods. This report is exclusively for the use of the be reproduced except in full without the written consent of our company. Test results transmitted herein are only applicable to the actual samples te and are not necessarily indicative of the properties of other apparently similar or identical materials.

## **Appendix C**

### Daily Project Field Records





# FIELD DENSITY TEST REPORT

Report Number: 04131111.0005  
Service Date: 03/26/14  
Report Date: 03/28/14  
Task:

# Terracon

9522 E. 47th Pl. Unit D  
Tulsa, OK 74145  
918-250-0461

## Client

Garver  
Attn: Ron Petrie  
2049 E. Joyce Blvd. Ste 400  
Fayetteville, AR 72703-5394

## Project

Tyson Parkway Extension  
I-540 & Don Tyson Parkway  
Springdale, AR

Project Number: 04131111

## Material Information

Mat. No.	Proctor Ref. No.	Classification and Description	Laboratory Test Method	Lab Test Data		Project Requirements	
				Optimum Water Content (%)	Max. Lab Density (pcf)	Water Content (%)	Compaction (%)
1	04129999.0001	Lime treated light brown fat clay		18.3	105.5	16.3 - 20.3	Min 95

## Field Test Data

Test No.	Test Location	Lift / Elev.	Mat. No.	Probe Depth (in)	Wet Density (pcf)	Water Content (pcf)	Water Content (%)	Dry Density (pcf)	Percent Compaction (%)
<b>Ramp #4</b>									
1	188+25	-12"	1	6	125.2	18.1	16.9	107.1	102
2	187+25	-12"	1	6	124.8	18.1	17.0	106.7	101
3	187+50	-6"	1	6	123.8	18.2	17.2	105.6	100
4	188+75	-6"	1	6	125.2	18.3	17.1	106.9	101

Datum:

Serial No:

Comments: Test and/or retest results on this report meet project requirements as noted above.

## Services:

Terracon Rep.: Joseph K. Rock  
Reported To: Justin Smith with Emery Sapp

Contractor:

Report Distribution:

(1) Garver

Start/Stop: 0000-0700

Reviewed By:



Justin Cox  
Staff Materials Engineer

Test Methods: \*, ASTM D6938

The tests were performed in general accordance with applicable ASTM, AASHTO, or DOT test methods. This report is exclusively for the use of the client indicated above and shall not be reproduced except in full without the written consent of our company. Test results transmitted herein are only applicable to the actual samples tested at the location(s) referenced and are not necessarily indicative of the properties of other apparently similar or identical materials.

# FIELD DENSITY TEST REPORT

Report Number: 04131111.0007  
Service Date: 03/27/14  
Report Date: 03/28/14  
Task:

# Terracon

9522 E. 47th Pl. Unit D  
Tulsa, OK 74145  
918-250-0461

## Client

Garver  
Attn: Ron Petrie  
2049 E. Joyce Blvd. Ste 400  
Fayetteville, AR 72703-5394

## Project

Tyson Parkway Extension  
I-540 & Don Tyson Parkway  
Springdale, AR

Project Number: 04131111

## Material Information

Mat. No.	Proctor Ref. No.	Classification and Description	Laboratory Test Method	Lab Test Data		Project Requirements	
				Optimum Water Content (%)	Max. Lab Density (pcf)	Water Content (%)	Compaction (%)
1	04131111.0001	Subgrade	AASHTO T180	18.3	105.5	16.3 - 20.3	Min 95
2	04129999.0001	Lime treated light brown fat clay		18.3	105.5	16.3 - 20.3	Min 95

## Field Test Data

Test No.	Test Location	Lift / Elev.	Mat. No.	Probe Depth (in)	Wet Density (pcf)	Water Content (pcf)	Water Content (%)	Dry Density (pcf)	Percent Compaction (%)
<b>Ramp #4</b>									
1	Station 188+20	SG	2	6	120.6	19.8	19.6	100.8	96
2	Station 187+00	SG	2	6	125.2	19.8	18.8	105.4	100
3	Station 186+10	SG	2	6	121.1	18.4	17.9	102.7	97

Datum:

Serial No:

Comments: Test and/or retest results on this report meet project requirements as noted above.

## Services:


Terracon Rep.: Anthony Reinking  
Reported To: Justin Smith with Emery Sapp

Contractor:

Report Distribution:

(1) Garver

Reviewed By:

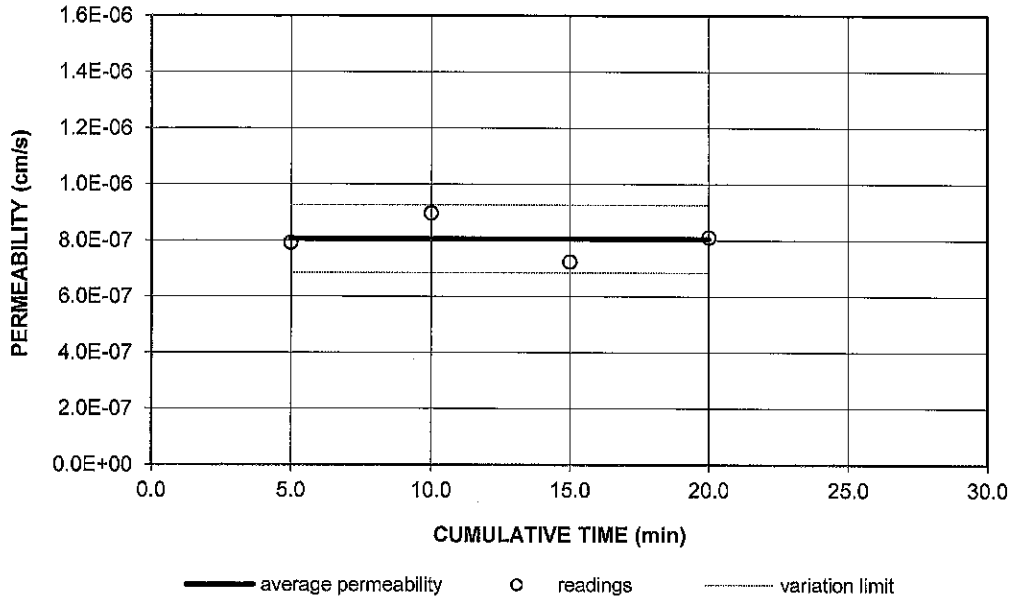
  
Justin Cox  
Staff Materials Engineer

Test Methods: \*, ASTM D6938

The tests were performed in general accordance with applicable ASTM, AASHTO, or DOT test methods. This report is exclusively for the use of the client indicated above and shall not be reproduced except in full without the written consent of our company. Test results transmitted herein are only applicable to the actual samples tested at the location(s) referenced and are not necessarily indicative of the properties of other apparently similar or identical materials.

**Appendix D**  
Compacted Clay Cover Pre-Construction  
Test Results

## FLEXIBLE WALL PERMEABILITY TEST



Test Specification:      ASTM D 5084 Method F

Fluid Temp. (°C)	Elapsed Time (min.)	Cumulative Time (min.)	Gradient (cm-Hg)	Calculated Permeability (cm/sec)	Average Permeability (cm/sec)
21.00	5.00	5.00	5.00	7.92E-07	<b>8.1E-07</b>
21.00	5.00	10.00	1.48	8.97E-07	
21.00	5.00	15.00	0.56	7.23E-07	
21.00	5.00	20.00	0.19	8.10E-07	

Compaction Data		Sample Data		Initial	Final
Proctor (pcf)	110.1	Specimen Height, (inches)		3.00	3.00
Opti. M.C., (%)	14.0	Specimen Diameter, (inches)		4.00	4.00
Comp. Method		Specimen Volume, (cu. in.)		37.68	37.68
% Recompt.	95.0	Moisture Content, (%)		14.15	22.82
Test Pressures (psi)		Percent Saturation (%)		62.32	100.00
Backpressure	90.00	Wet Mass Density (pcf)		119.24	128.30
Cell pressure	95.00	Dry Mass Density (pcf)		104.46	104.46
Eff. Stress	<b>5.00</b>	Void Ratio		0.61	0.62
Specific Gravity	2.70	Calculated Porosity, %		38.00	38.12

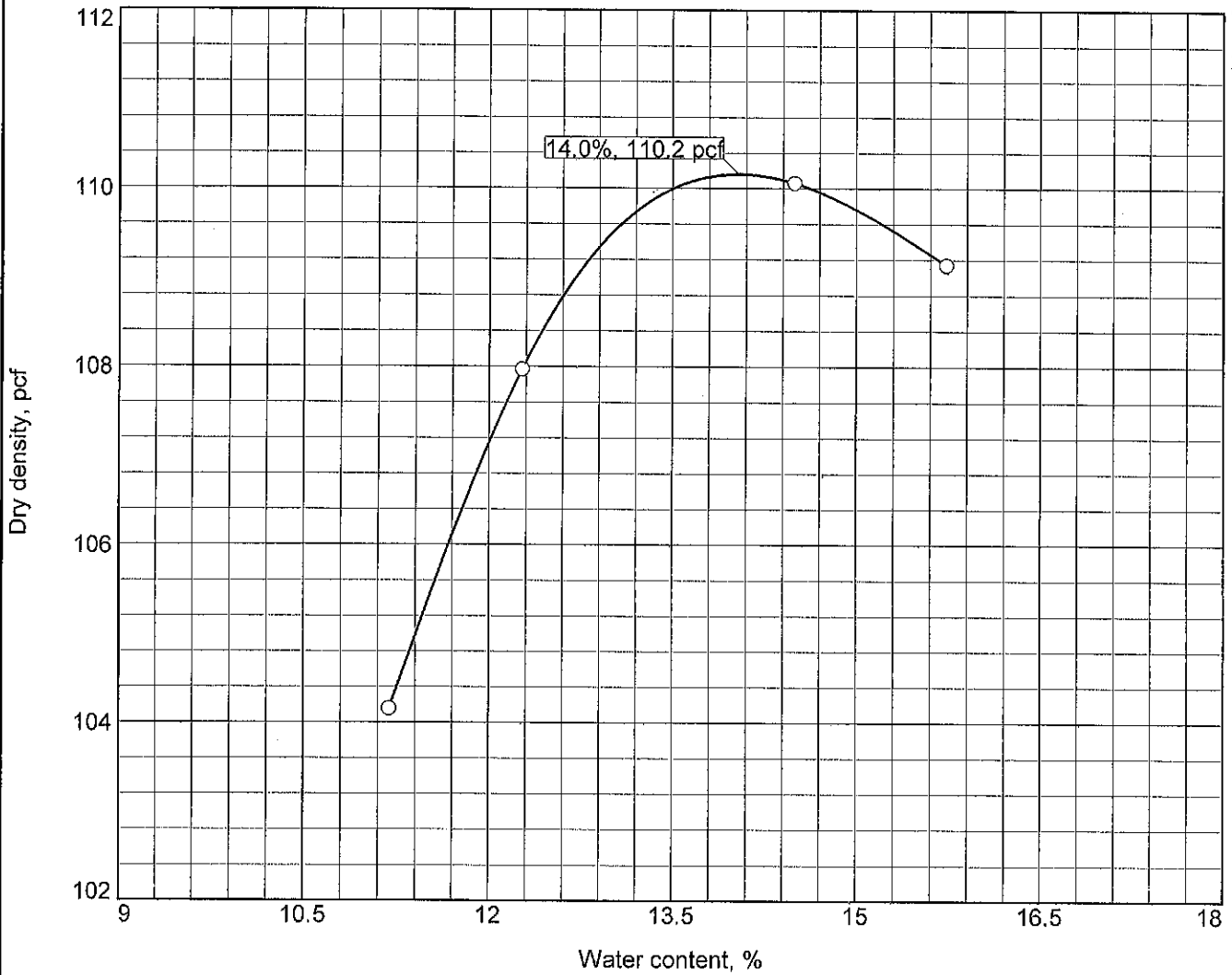
USCS                      SG Assumed      LL                                      PI  
 Permeant Used:      WATER      Remarks      BROWN LEAN CLAY

Project Name	Tyson Parkway Extension	Tested by	FCE	Reviewed by	TGG
Client	Garver      W.O.#      35139161	<b>FLEXIBLE WALL PERMEABILITY TEST</b> 			
Sample Number	North Stockpile				
Sample Location	Cobblewood      0-5'				
Date	10/21/2013      Lab No.      6456				



# COMPACTION TEST REPORT

ZAV for  
Sp.G. =  
2.70



Test specification: ASTM D 698-07 Method B Standard

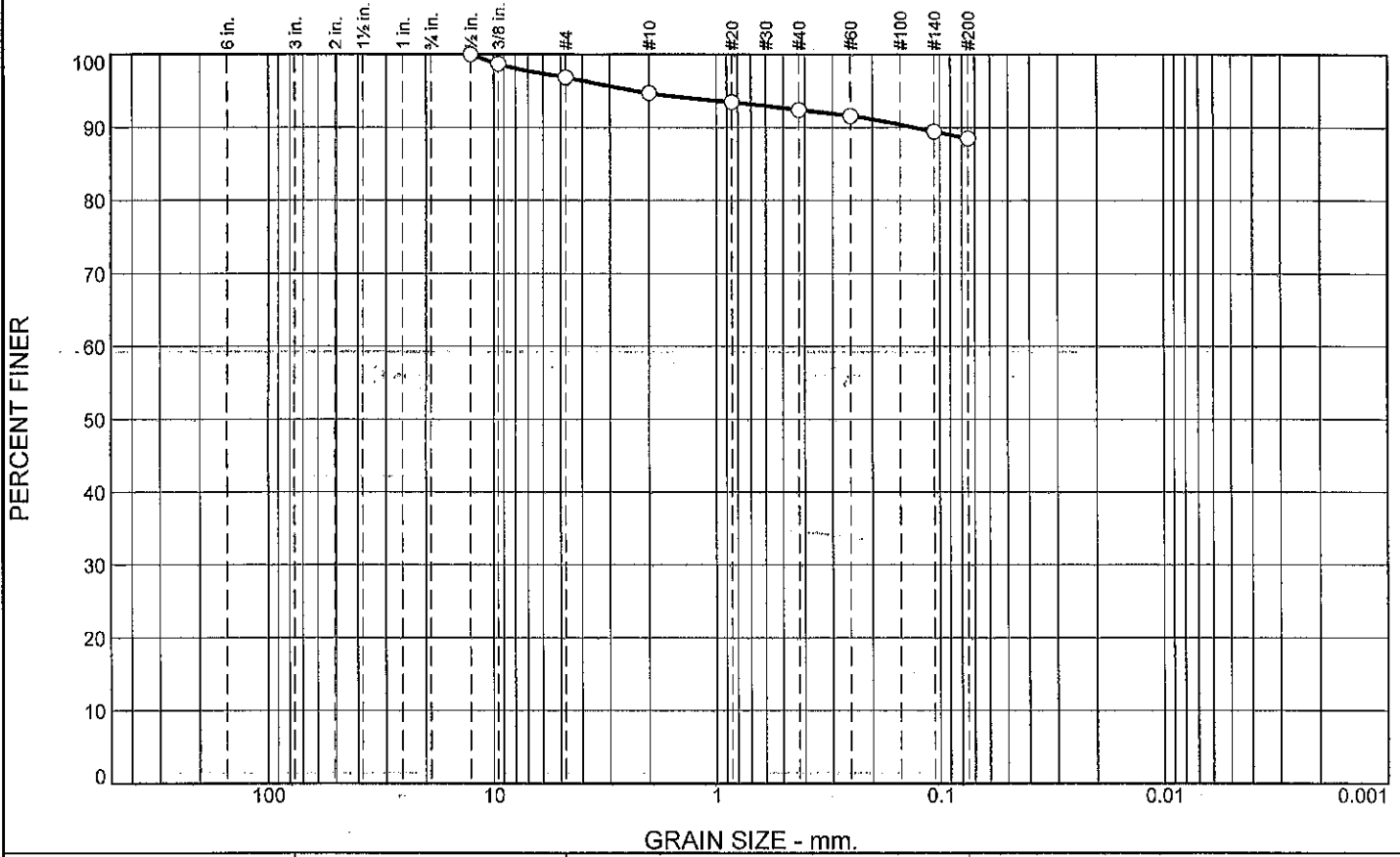
Elev/ Depth	Classification		Nat. Moist.	Sp.G.	LL	PI	% > 3/8 in.	% < No.200
	USCS	AASHTO						
	CL	A-6(13)	18.8	2.70	32	16	1.3	88.5

TEST RESULTS	MATERIAL DESCRIPTION
Maximum dry density = 110.2 pcf Optimum moisture = 14.0 %	BROWN LEAN CLAY
Project No. 35139161    Client: GARVER Project: TYSON PARKWAY EXTENSION Source of Sample: 6456	Remarks: SOURCE: COBBLESTONE - NORTH STOCKPILE
<b>Terracon, Inc.</b> Cincinnati, Ohio	Exhibit    6456

Tested By: MRM

Checked By: GS

# Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	3.2	2.1	2.3	3.9	88.5	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
.5	100.0		
.375	98.7		
#4	96.8		
#10	94.7		
#20	93.5		
#40	92.4		
#60	91.6		
#140	89.5		
#200	88.5		

**Material Description**

BROWN LEAN CLAY

SOURCE: COBBLESTONE - NORTH STOCKPILE

**Atterberg Limits**

PL= 16      LL= 32      PI= 16

**Coefficients**

D<sub>90</sub>= 0.1278      D<sub>85</sub>=      D<sub>60</sub>=  
D<sub>50</sub>=      D<sub>30</sub>=      D<sub>15</sub>=  
D<sub>10</sub>=      C<sub>u</sub>=      C<sub>c</sub>=

**Classification**

USCS= CL      AASHTO= A-6(13)

**Remarks**

WC=18.8%

\* (no specification provided)

Source of Sample: 6456

Date: 10-15-13

Terracon, Inc.

Cincinnati, Ohio

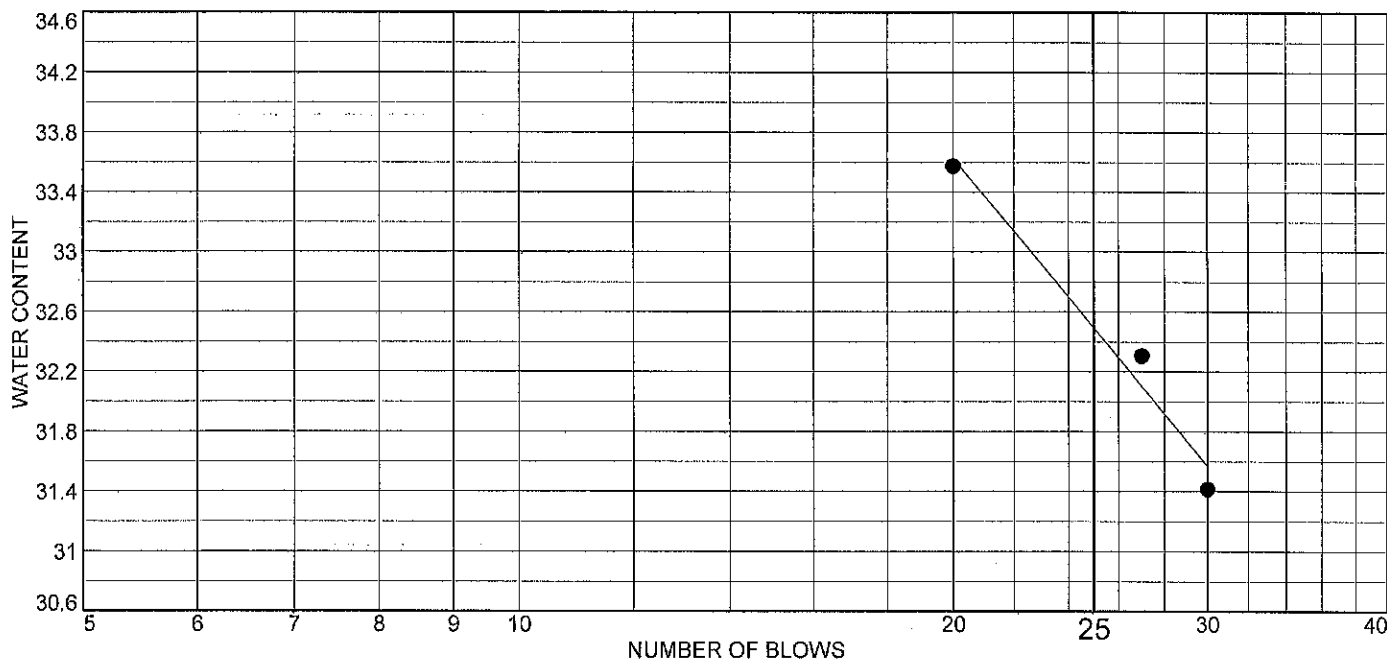
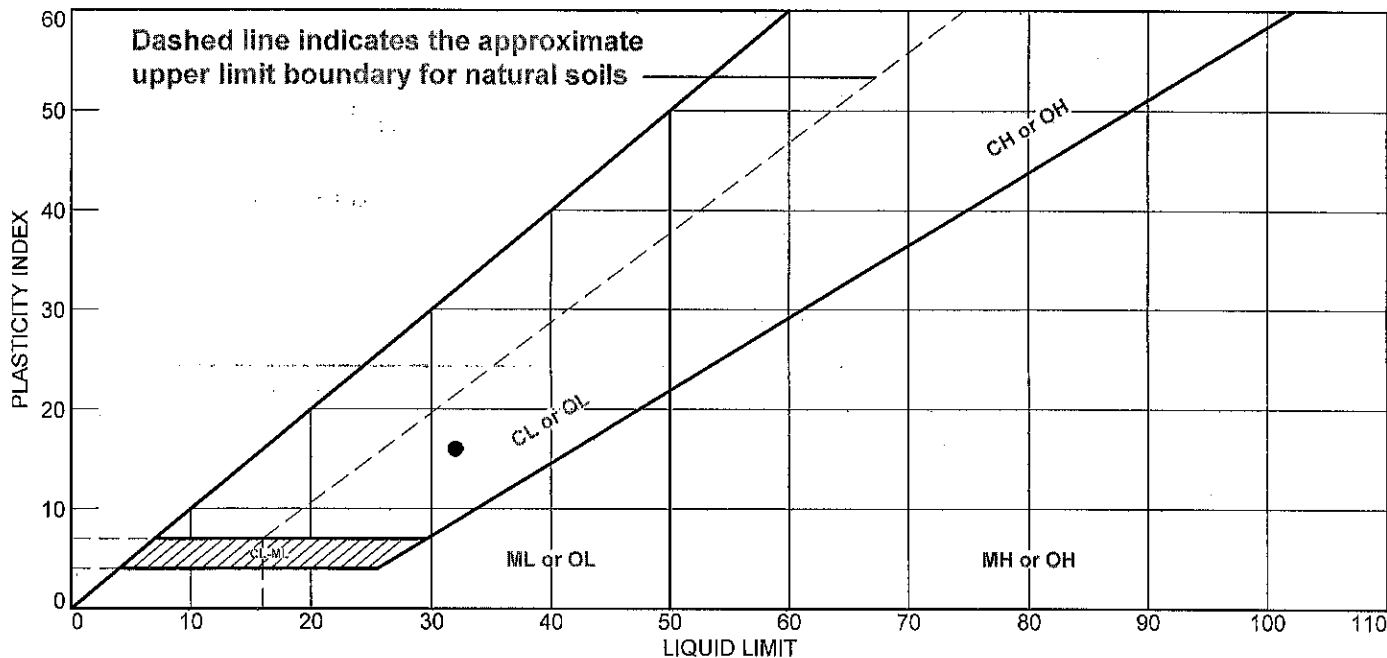
Client: GARVER  
Project: TYSON PARKWAY EXTENSION

Project No: 35139161      Exhibit 6456

Tested By: DR

Checked By: GS

# LIQUID AND PLASTIC LIMITS TEST REPORT



MATERIAL DESCRIPTION	LL	PL	PI	%<#40	%<#200	USCS
BROWN LEAN CLAY	32	16	16	92.4	88.5	CL
SOURCE: COBBLESTONE - NORTH STOCKPILE						

Project No. 35139161      Client: GARVER  
 Project: TYSON PARKWAY EXTENSION  
 Source of Sample: 6456

Remarks:  
 • WC=18.8%

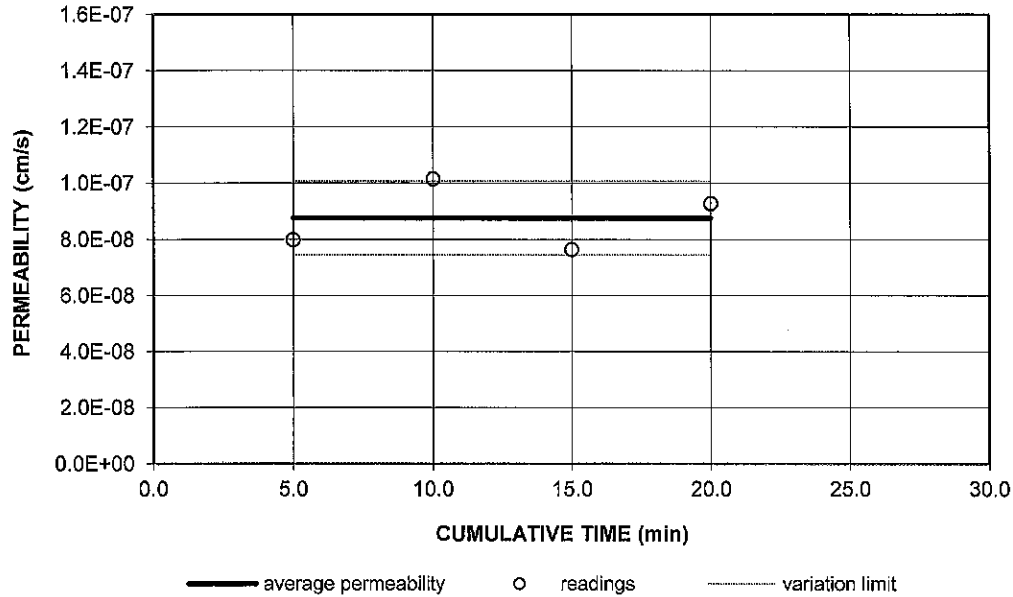
Exhibit    6456

**Terracon, Inc.**  
 Cincinnati, Ohio

Tested By: JK

Checked By: GS

## FLEXIBLE WALL PERMEABILITY TEST



Test Specification:      ASTM D 5084 Method F

Fluid Temp. (°C)	Elapsed Time (min.)	Cumulative Time (min.)	Gradient (cm-Hg)	Calculated Permeability (cm/sec)	Average Permeability (cm/sec)
21.00	5.00	5.00	12.97	7.98E-08	<b>8.8E-08</b>
21.00	5.00	10.00	11.30	1.01E-07	
21.00	5.00	15.00	10.19	7.64E-08	
21.00	5.00	20.00	8.98	9.27E-08	

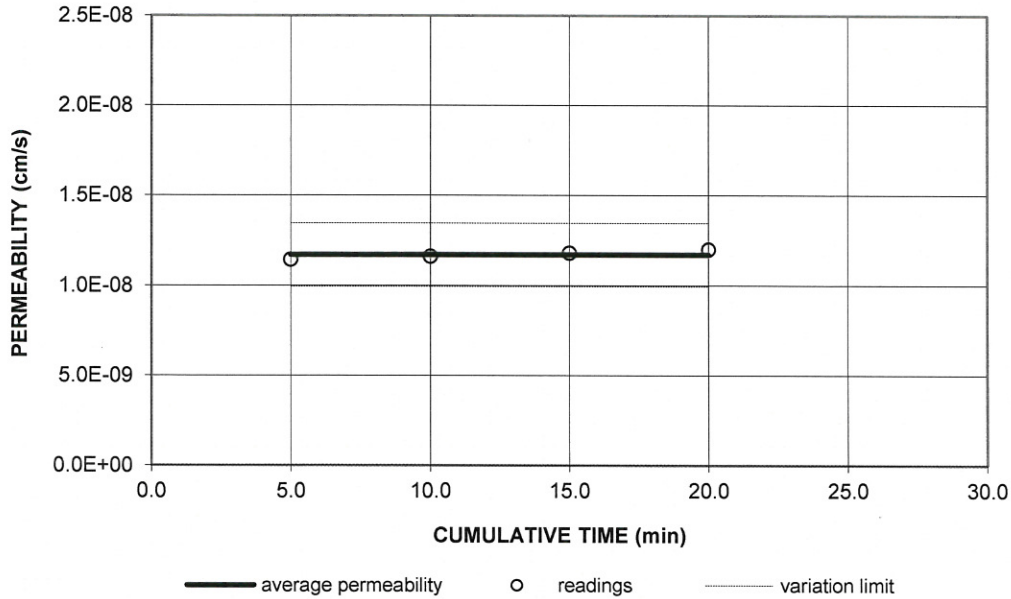
Compaction Data		Sample Data		Initial	Final
Proctor (pcf)	110.1	Specimen Height, (inches)		3.00	3.00
Opti. M.C., (%)	14.0	Specimen Diameter, (inches)		4.00	4.00
Comp. Method		Specimen Volume, (cu. In.)		37.68	37.68
% Recompt.	99.0	Moisture Content, (%)		16.04	19.42
Test Pressures (psi)		Percent Saturation (%)		79.28	95.97
Backpressure	90.00	Wet Mass Density (pcf)		126.44	130.12
Cell pressure	95.00	Dry Mass Density (pcf)		108.96	108.96
Eff. Stress	5.00	Void Ratio		0.55	0.55
Specific Gravity	2.70	Calculated Porosity, %		35.33	35.33

USCS	SG Assumed	LL	PI
Permeant Used:	WATER	Remarks	BROWN LEAN CLAY

Project Name	Tyson Parkway Extension	Tested by	FCE	Reviewed by	TGG
Client	Garver      W.O.#      35139161	<b>FLEXIBLE WALL PERMEABILITY TEST</b> 			
Sample Number	North Stockpile				
Sample Location	Cobblewood      0-5'				
Date	10/28/2013      Lab No.      6456rr				

**Appendix E**  
Compacted Clay Cover Construction  
Test Results

## FLEXIBLE WALL PERMEABILITY TEST



Test Specification: ASTM D 5084 Method F

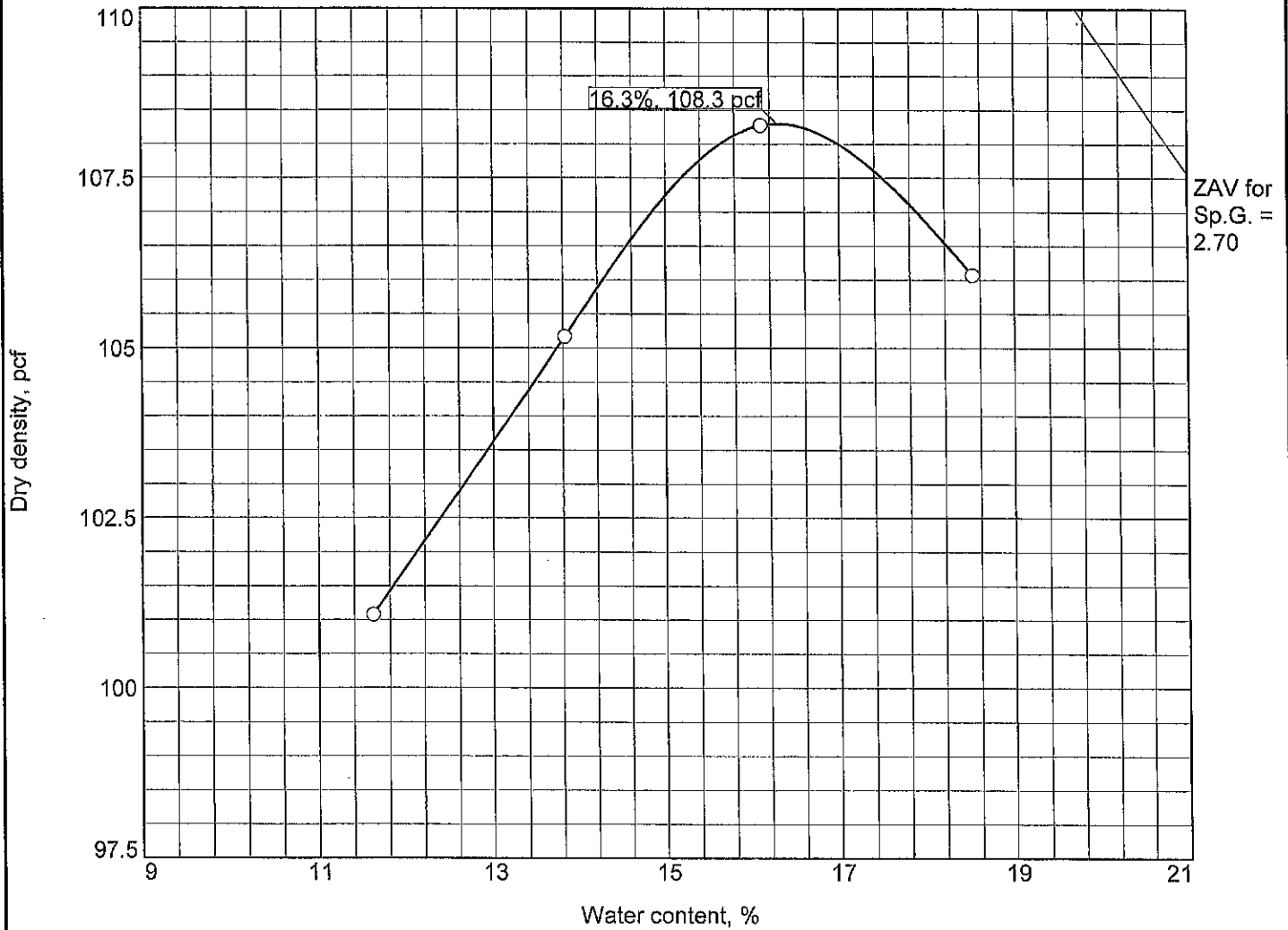
Fluid Temp. (°C)	Elapsed Time (min.)	Cumulative Time (min.)	Gradient (cm-Hg)	Calculated Permeability (cm/sec)	Average Permeability (cm/sec)
21.00	5.00	5.00	11.86	1.14E-08	<b>1.2E-08</b>
21.00	5.00	10.00	11.67	1.16E-08	
21.00	5.00	15.00	11.48	1.18E-08	
21.00	5.00	20.00	11.30	1.20E-08	

Compaction Data		Sample Data		Initial	Final
Proctor (pcf)	108.3	Specimen Height, (inches)		3.00	3.01
Opti. M.C., (%)	16.3	Specimen Diameter, (inches)		4.00	4.00
Comp. Method		Specimen Volume, (cu. In.)		37.68	37.81
% Recompt.	100.0	Moisture Content, (%)		18.50	20.41
Test Pressures (psi)		Percent Saturation (%)		90.61	99.03
Backpressure	90.00	Wet Mass Density (pcf)		128.70	130.34
Cell pressure	93.00	Dry Mass Density (pcf)		108.61	108.25
Eff. Stress	3.00	Void Ratio		0.55	0.56
Specific Gravity	2.70	Calculated Porosity, %		35.54	35.75

USCS: SG Assumed LL PI  
 Permeant Used: WATER Remarks: BR SANDY LEAN CLAY W/GRAVEL

Project Name	Tyson Parkway Extension	Tested by	FCE	Reviewed by	TGG
Client	Garver W.O.# 35139161	<b>FLEXIBLE WALL PERMEABILITY TEST</b> 			
Sample Number	#2				
Sample Location	Cobble				
Date	11/11/2013 Lab No. 6934				

# COMPACTION TEST REPORT



Test specification: ASTM D 698-07 Method A Standard

Elev/ Depth	Classification		Nat. Moist.	Sp.G.	LL	PI	% > #4	% < No.200
	USCS	AASHTO						
	CL	A-6(5)	20.1	2.70	31	14	17.2	59.3

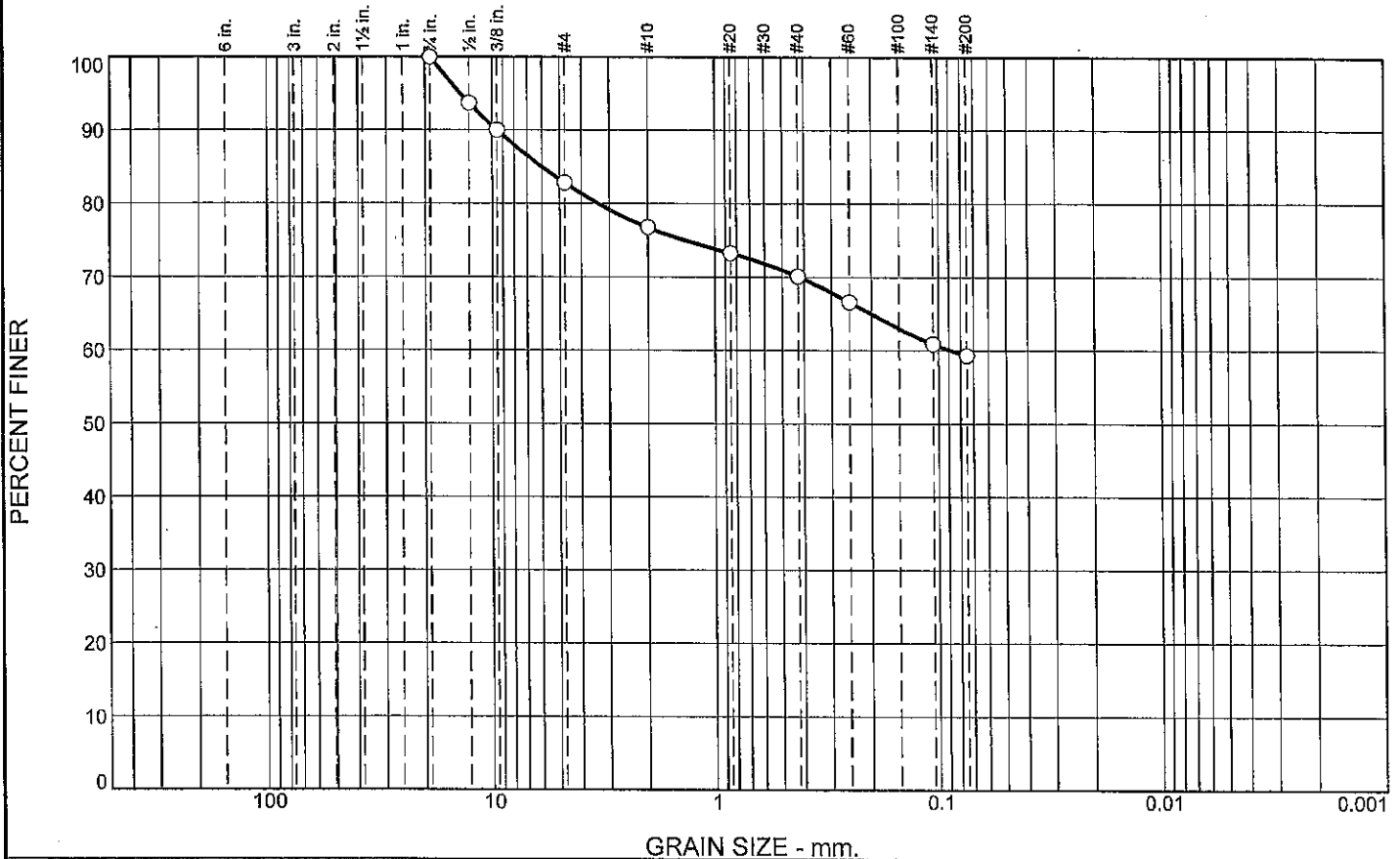
TEST RESULTS	MATERIAL DESCRIPTION
Maximum dry density = 108.3 pcf Optimum moisture = 16.3 %	BROWN SANDY LEAN CLAY WITH GRAVEL
Project No. 35139161    Client: GARVER Project: TYSON PARKWAY EXTENSION Source of Sample: Construction    Sample Number: Comp. from Cobble	Remarks: Obtained by S. Billingsly Date obtained 10-25-13
<b>Terracon, Inc.</b> Cincinnati, Ohio	Exhibit    6934

Tested By: LH

Checked By: GS



# Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	17.2	6.0	6.7	10.8	59.3	

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
.75	100.0		
.5	93.7		
.375	90.0		
#4	82.8		
#10	76.8		
#20	73.3		
#40	70.1		
#60	66.7		
#140	60.9		
#200	59.3		

**Material Description**

BROWN SANDY LEAN CLAY WITH GRAVEL

**Atterberg Limits**

PL= 17      LL= 31      PI= 14

**Coefficients**

D<sub>90</sub>= 9.5460      D<sub>85</sub>= 6.0081      D<sub>60</sub>= 0.0873  
D<sub>50</sub>=              D<sub>30</sub>=              D<sub>15</sub>=  
D<sub>10</sub>=              C<sub>u</sub>=              C<sub>c</sub>=

**Classification**

USCS= CL              AASHTO= A-6(5)

**Remarks**

WC=20.1%

\* (no specification provided)

Source of Sample: Construction  
Sample Number: Comp. from Cobble

Date: 11-13-13

**Terracon, Inc.**

Cincinnati, Ohio

Client: GARVER  
Project: TYSON PARKWAY EXTENSION

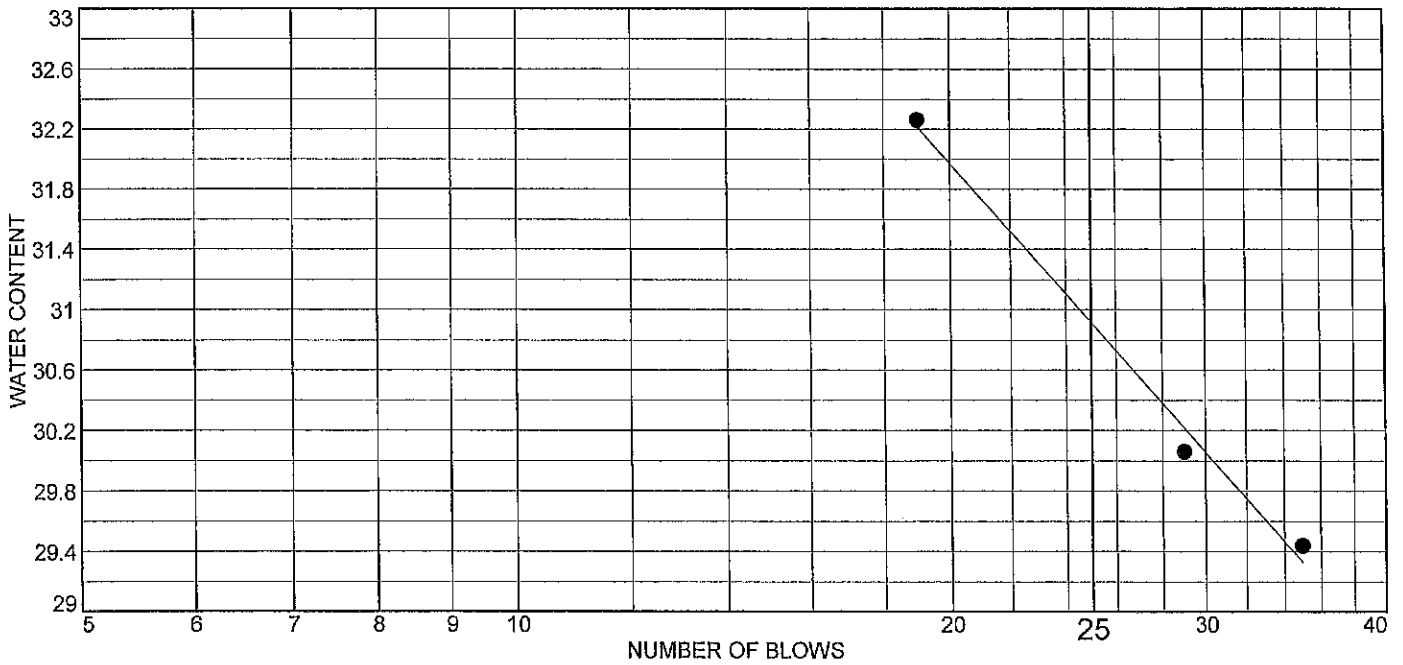
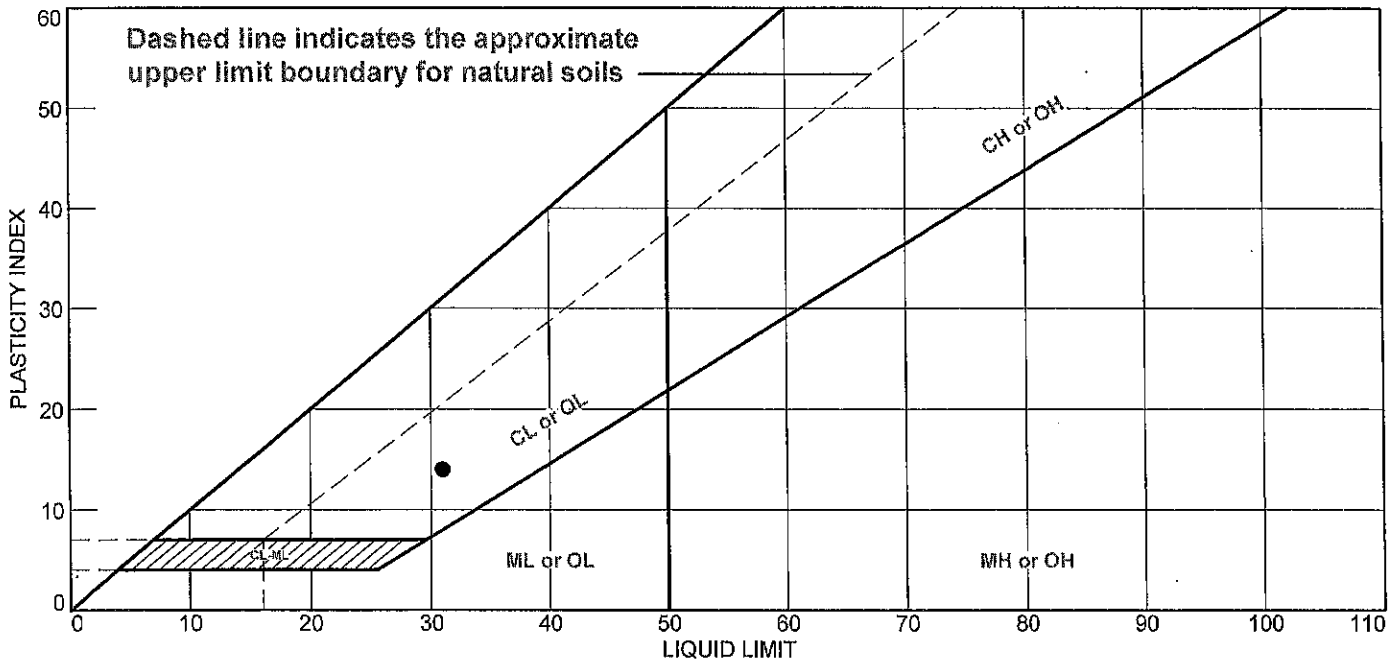
Project No: 35139161

Exhibit 6934

Tested By: DR

Checked By: GS

# LIQUID AND PLASTIC LIMITS TEST REPORT



MATERIAL DESCRIPTION	LL	PL	PI	%<#40	%<#200	USCS
• BROWN SANDY LEAN CLAY WITH GRAVEL	31	17	14	70.1	59.3	CL

Project No. 35139161 Client: GARVER

Project: TYSON PARKWAY EXTENSION

Source of Sample: Construction  
Sample Number: Comp. from Cobble

Remarks:

• WC=20.1%

**Terracon, Inc.**

Cincinnati, Ohio

Exhibit 6934

Checked By: GS

# LABORATORY COMPACTION CHARACTERISTICS OF SOIL REPORT



Report Number: 35139161.0001

Service Date: 03/24/14

Report Date: 03/24/14

25809 I-30 South  
Bryant, AR 72022  
501-847-9292

## Client

Garver  
Attn: Ron Petrie  
2049 E. Joyce Blvd. Ste 400  
Fayetteville, AR 72703-5394

## Project

Tyson Parkway Extension  
Don Tyson Parkway and Interstate 540  
Springdale, AR

Project Number 35139161

## Material Information

Source of Material: On-site Fill  
Proposed Use: Fill

## Sample Information

Sample Date: 03/21/14  
Sampled By: Gramling, Paul  
Sample Location: On-site

Sample Description: PENDING PROCTOR

## Laboratory Test Data

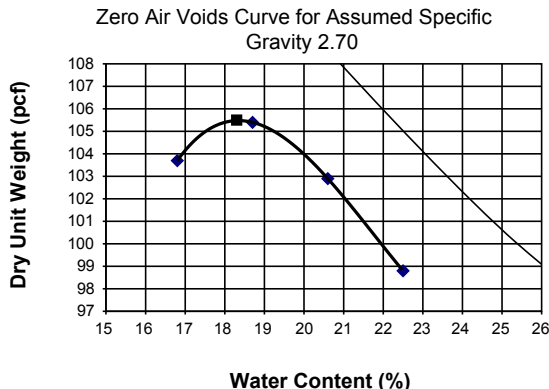
Test Procedure: ASTM D698  
Test Method: Method B  
Sample Preparation: Wet  
Rammer Type: Manual  
Maximum Dry Unit Weight (pcf): 105.5  
Optimum Water Content (%): 18.3

Liquid Limit:  
Plastic Limit:  
Plasticity Index:  
In-Place Moisture (%):

Result

Specifications

USCS:



Comments:

Services:

Terracon Rep.:

Reported To:

Contractor:

Report Distribution:

(1) Garver, Ron Petrie

Reviewed By: \_\_\_\_\_

William Butler  
Senior Staff Engineer

Test Methods: AASHTO T99

The tests were performed in general accordance with applicable ASTM, AASHTO, or DOT test methods. This report is exclusively for the use of the be reproduced except in full without the written consent of our company. Test results transmitted herein are only applicable to the actual samples te and are not necessarily indicative of the properties of other apparently similar or identical materials.

# LABORATORY COMPACTION CHARACTERISTICS OF SOIL REPORT



Report Number: 35139161.0001

Service Date: 03/24/14

Report Date: 03/24/14

25809 I-30 South  
Bryant, AR 72022  
501-847-9292

## Client

Garver  
Attn: Ron Petrie  
2049 E. Joyce Blvd. Ste 400  
Fayetteville, AR 72703-5394

## Project

Tyson Parkway Extension  
Don Tyson Parkway and Interstate 540  
Springdale, AR

Project Number 35139161

## Material Information

Source of Material: On-site Fill  
Proposed Use: Fill

## Sample Information

Sample Date: 03/21/14  
Sampled By: Gramling, Paul  
Sample Location: On-site

Sample Description: PENDING PROCTOR

## Laboratory Test Data

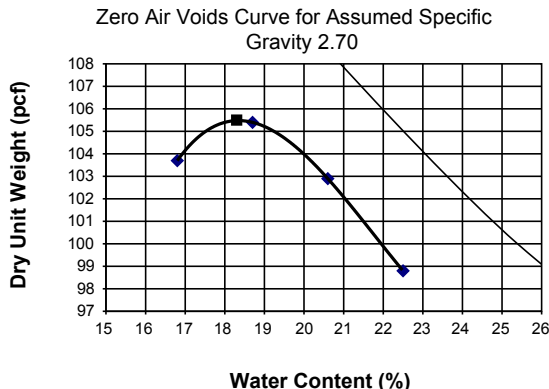
Test Procedure: ASTM D698  
Test Method: Method B  
Sample Preparation: Wet  
Rammer Type: Manual  
Maximum Dry Unit Weight (pcf): 105.5  
Optimum Water Content (%): 18.3

Liquid Limit:  
Plastic Limit:  
Plasticity Index:  
In-Place Moisture (%):

Result

Specifications

USCS:



Comments:

Services:

Terracon Rep.:

Reported To:

Contractor:

Report Distribution:

(1) Garver, Ron Petrie

Reviewed By: \_\_\_\_\_

William Butler  
Senior Staff Engineer

Test Methods: AASHTO T99

The tests were performed in general accordance with applicable ASTM, AASHTO, or DOT test methods. This report is exclusively for the use of the be reproduced except in full without the written consent of our company. Test results transmitted herein are only applicable to the actual samples te and are not necessarily indicative of the properties of other apparently similar or identical materials.

## **Appendix F**

### Field Moisture/Density Test Results





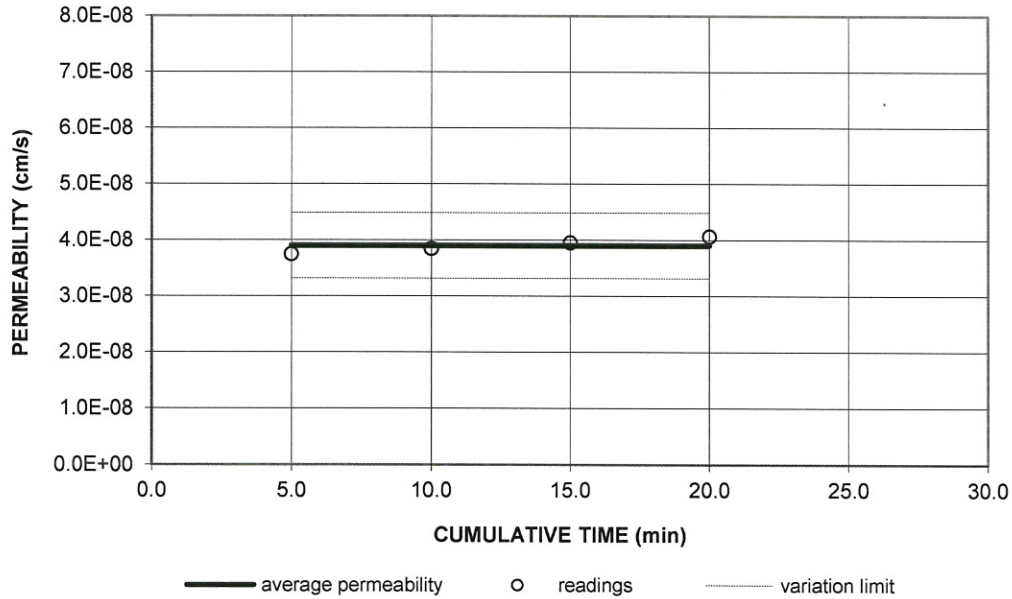




# **Appendix G**

## Compacted Clay Cover Permeability Test Results

## FLEXIBLE WALL PERMEABILITY TEST



Test Specification: ASTM D 5084 Method F

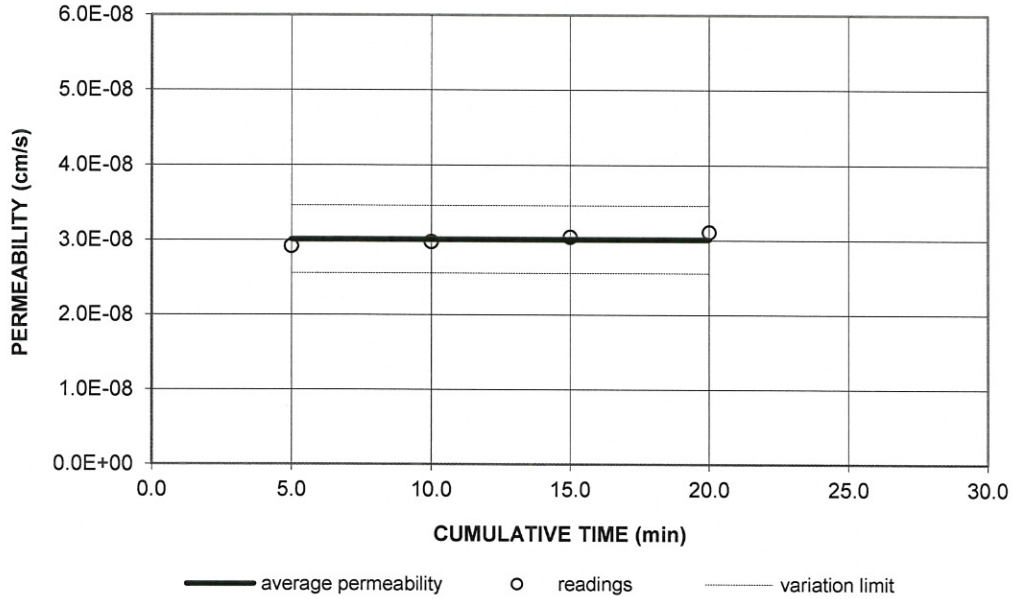
Fluid Temp. (°C)	Elapsed Time (min.)	Cumulative Time (min.)	Gradient (cm-Hg)	Calculated Permeability (cm/sec)	Average Permeability (cm/sec)
21.00	5.00	5.00	14.40	3.74E-08	<b>3.9E-08</b>
21.00	5.00	10.00	14.02	3.84E-08	
21.00	5.00	15.00	13.64	3.95E-08	
21.00	5.00	20.00	13.26	4.06E-08	

Compaction Data		Sample Data		Initial	Final
Proctor (pcf)		Specimen Height, (inches)		2.93	2.91
Opti. M.C., (%)		Specimen Diameter, (inches)		2.83	2.83
Comp. Method		Specimen Volume, (cu. In.)		18.43	18.29
% Recompt.		Moisture Content, (%)		19.95	20.39
Test Pressures (psi)		Percent Saturation (%)		92.02	95.89
Backpressure	90.00	Wet Mass Density (pcf)		127.47	128.85
Cell pressure	93.00	Dry Mass Density (pcf)		106.27	107.03
<b>Eff. Stress</b>	<b>3.00</b>	Void Ratio		0.59	0.57
Specific Gravity	2.70	Calculated Porosity, %		36.93	36.47

USCS	SG Assumed	LL	PI
Permeant Used:	WATER	Remarks	BROWN SANDY LEAN CLAY W/ GRAVEL

Project Name	Tyson Parkway Extension	Tested by	FCE	Reviewed by	TGG
Client	Garver W.O.# 35139161	<b>FLEXIBLE WALL PERMEABILITY TEST</b> 			
Sample Number	P-1				
Sample Location					
Date	10/31/2013 Lab No. 6935				

## FLEXIBLE WALL PERMEABILITY TEST



Test Specification: ASTM D 5084 Method F

Fluid Temp. (°C)	Elapsed Time (min.)	Cumulative Time (min.)	Gradient (cm-Hg)	Calculated Permeability (cm/sec)	Average Permeability (cm/sec)
21.00	5.00	5.00	13.86	2.92E-08	<b>3.0E-08</b>
21.00	5.00	10.00	13.58	2.98E-08	
21.00	5.00	15.00	13.29	3.04E-08	
21.00	5.00	20.00	13.00	3.11E-08	

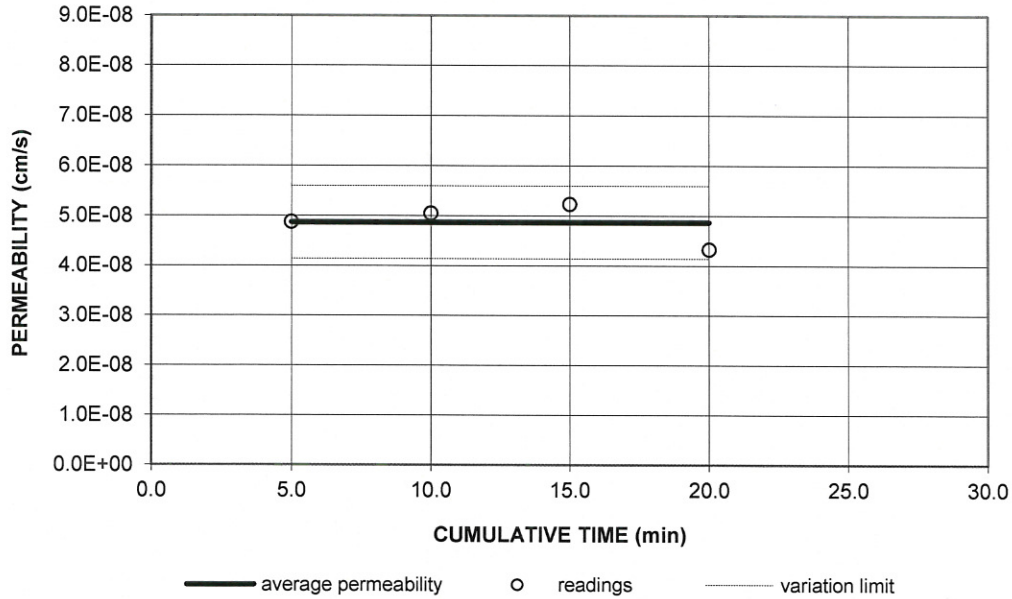
Compaction Data		Sample Data		Initial	Final
Proctor (pcf)		Specimen Height, (inches)		2.91	2.85
Opti. M.C., (%)		Specimen Diameter, (inches)		2.83	2.83
Comp. Method		Specimen Volume, (cu. In.)		18.31	17.98
% Recompt.		Moisture Content, (%)		20.97	20.39
Test Pressures (psi)		Percent Saturation (%)		96.64	98.76
Backpressure	90.00	Wet Mass Density (pcf)		128.52	130.23
Cell pressure	93.00	Dry Mass Density (pcf)		106.24	108.18
<b>Eff. Stress</b>	<b>3.00</b>	Void Ratio		0.59	0.56
Specific Gravity	2.70	Calculated Porosity, %		36.94	35.79

USCS	SG Assumed	LL	PI
Permeant Used:	WATER	Remarks	BROWN SANDY LEAN CLAY W/ GRAVEL

Project Name	Tyson Parkway Extension	Tested by	FCE	Reviewed by	TGG
Client	Garver W.O.# 35139161	<b>FLEXIBLE WALL PERMEABILITY TEST</b> 			
Sample Number	P-2				
Sample Location					
Date	10/31/2013 Lab No. 6936				



## FLEXIBLE WALL PERMEABILITY TEST



Test Specification:      ASTM D 5084 Method F

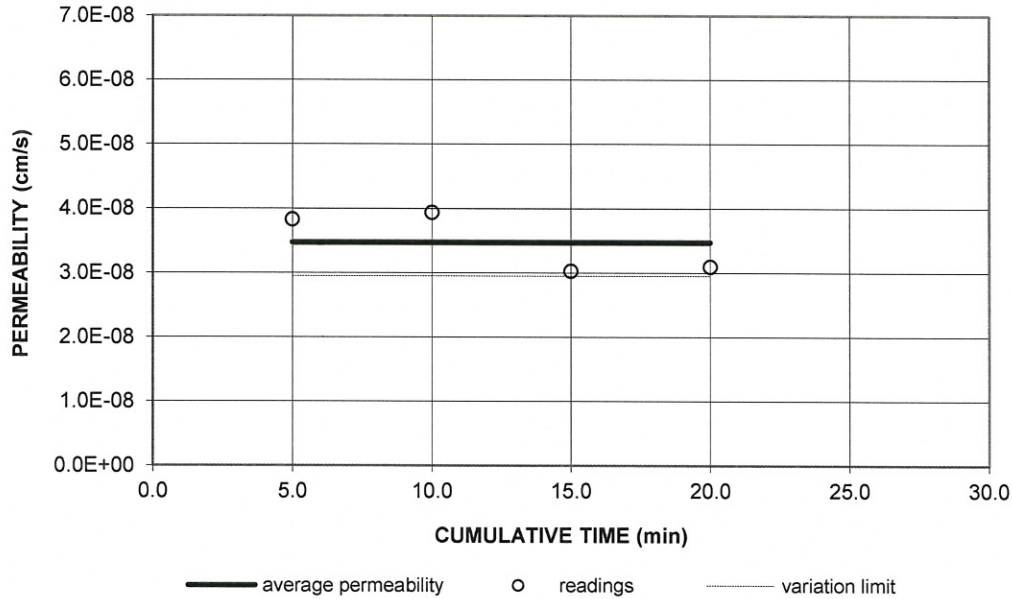
Fluid Temp. (°C)	Elapsed Time (min.)	Cumulative Time (min.)	Gradient (cm-Hg)	Calculated Permeability (cm/sec)	Average Permeability (cm/sec)
21.00	5.00	5.00	14.05	4.87E-08	<b>4.9E-08</b>
21.00	5.00	10.00	13.56	5.05E-08	
21.00	5.00	15.00	13.08	5.23E-08	
21.00	5.00	20.00	12.69	4.32E-08	

Compaction Data		Sample Data		Initial	Final
Proctor (pcf)		Specimen Height, (inches)		2.87	2.81
Opti. M.C., (%)		Specimen Diameter, (inches)		2.80	2.80
Comp. Method		Specimen Volume, (cu. In.)		17.66	17.32
% Recompt.		Moisture Content, (%)		20.57	20.46
Test Pressures (psi)		Percent Saturation (%)		94.77	99.42
Backpressure	90.00	Wet Mass Density (pcf)		128.07	130.46
Cell pressure	93.00	Dry Mass Density (pcf)		106.22	108.30
<b>Eff. Stress</b>	<b>3.00</b>	Void Ratio		0.59	0.56
Specific Gravity	2.70	Calculated Porosity, %		36.95	35.72

USCS	SG Assumed	LL	PI
Permeant Used:	WATER	Remarks	BROWN SANDY LEAN CLAY W/ GRAVEL

Project Name	Tyson Parkway Extension	Tested by	FCE	Reviewed by	TGG
Client	Garver      W.O.#      35139161	<b>FLEXIBLE WALL PERMEABILITY TEST</b> 			
Sample Number	P-3				
Sample Location					
Date	10/31/2013      Lab No.      6937				

## FLEXIBLE WALL PERMEABILITY TEST



Test Specification: ASTM D 5084 Method F

Fluid Temp. (°C)	Elapsed Time (min.)	Cumulative Time (min.)	Gradient (cm-Hg)	Calculated Permeability (cm/sec)	Average Permeability (cm/sec)
21.00	5.00	5.00	14.02	3.83E-08	<b>3.5E-08</b>
21.00	5.00	10.00	13.63	3.94E-08	
21.00	5.00	15.00	13.34	3.03E-08	
21.00	5.00	20.00	13.05	3.09E-08	

Compaction Data		Sample Data		Initial	Final
Proctor (pcf)		Specimen Height, (inches)		2.85	2.75
Opti. M.C., (%)		Specimen Diameter, (inches)		2.83	2.83
Comp. Method		Specimen Volume, (cu. In.)		17.99	17.28
% Recompt.		Moisture Content, (%)		20.93	19.69
Test Pressures (psi)		Percent Saturation (%)		99.64	100.00
Backpressure	90.00	Wet Mass Density (pcf)		130.01	133.96
Cell pressure	93.00	Dry Mass Density (pcf)		107.50	111.93
<b>Eff. Stress</b>	<b>3.00</b>	Void Ratio		0.57	0.53
Specific Gravity	2.70	Calculated Porosity, %		36.19	34.71

USCS	SG Assumed	LL	PI
Permeant Used:	WATER	Remarks	BROWN SANDY LEAN CLAY W/ GRAVEL

Project Name	Tyson Parkway Extension	Tested by	FCE	Reviewed by	TGG
Client	Garver W.O.# 35139161	<b>FLEXIBLE WALL PERMEABILITY TEST</b> 			
Sample Number	P-4				
Sample Location					
Date	10/31/2013 Lab No. 6938				

## **Appendix H**

### Project Photographs





